

FINAL HYDROGEOLOGICAL ASSESSMENT REPORT CLARK AVENUE EXTENSION RUTHERFORD ROAD TO KENNEDY ROAD CITY OF BRAMPTON

Report

То

HDR Inc.

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1. INTRODUCTION

This report presents the results of a preliminary hydrogeological assessment completed by Thurber Engineering Ltd. (Thurber) in conjunction with a geotechnical investigation in support of the Municipal Class Environmental Assessment Study (EA) for the Clark Boulevard Extension and Eastern Avenue widening in the City of Brampton, Ontario. The limits of the project site are from Rutherford Road to Kennedy Road for a total length of approximately 900 m (the Site).

The project is expected to consist of the construction of a new 4-lane urban cross-section segment of Clark Boulevard between Rutherford Road and Hansen Road. This extension will also involve construction of a bridge or culvert for the crossing of a Spring Creek tributary. In addition, Eastern Avenue is to be widened from a 2-lane rural cross section to a 4-lane urban cross section.

The purpose of the Preliminary Hydrogeological Investigation Report is to conduct a preliminary assessment of the hydrogeological conditions, evaluation of potential construction dewatering requirements and methods, anticipated impacts, Permit To Take Water (PTTW) requirements, discharge requirements, and disposal options for groundwater collected from dewatering operations (including mitigation measures).

The hydrogeological components of the investigation included the following tasks:

- Measurement of groundwater levels on completion of installation and again afterwards once groundwater levels have stabilized;
- Conduct in-situ hydraulic conductivity testing at three of the installed monitoring wells; and,
- Collect groundwater samples for chemical testing in accordance with Peel Region Sewer Use Bylaws from the installed monitoring wells.

Note, a Ministry of the Environment, Conservation and Parks (MECP) water well search or doorto-door survey of private water supply wells was not completed as part of this preliminary assignment. Recommendations for further studies is presented herein.

It is a condition of this report that Thurber's performance of its professional services is subject to the attached Statement of Limitations and Conditions.

2. BACKGROUND REVIEW

2.1 Site Description

The existing alignment of Eastern Avenue from Kennedy Road to Hansen Avenue is an east-west arterial road under the jurisdiction of the City of Brampton (the City) and consists of a 2-lane rural cross-section with a posted speed limit of 50 km/hr. Eastern Avenue is currently classified as a minor arterial road with an ultimate right-of-way of 26 to 30 meters.



The existing Clark Boulevard, east of Rutherford Road is an east-west arterial road under the jurisdiction of the City and consists of a 4-lane urban cross-section with a posted speed limit of 50 km/hr. The proposed extension of Clark Boulevard is located at the westerly limit of Clark Boulevard and would extend to Hansen Road. This extension of Clark Boulevard would be classified as a minor arterial road with an ultimate right-of-way of 26 to 30 meters.

The Clark Boulevard extension would require a crossing of a tributary of Spring Creek. The crossing would be located approximate 125 m west of Rutherford Road South where the creek flows in an easterly direction. The recommendations include a channel re-alignment to permit a more perpendicular crossing of the channel.

The area of the proposed extension of Clark Boulevard east of the creek is currently occupied by a vacant parcel of industrial property owned by the City of Brampton at 25 Rutherford Road South. West of the creek the area of the extension is occupied by 35 Rutherford Road South, which currently contains a manufacturing plant for pre-fabricated concrete products.

The area surrounding the project corridor within 500 m of the Site (the Study Area) mainly consists of industrial properties along both sides of Eastern Avenue and the proposed Clark Boulevard extension. The Site and Study Area are shown on Figure 1.

2.2 Site Physiographic, Geologic and Hydrogeologic Settings

Based on the information in *The Physiography of Southern Ontario*¹ by Chapman and Putnam (1984), the Study Area is located within the Peel Plain physiographic region. The Peel Plain is characterized by a level to undulating topography gradually sloping towards Lake Ontario with surficial soil comprising a thin lacustrine clay underlain by till. The predominant physiographic landform within the study area is comprised of Bevelled Till Plains. A physiographic region map of the Study Area is shown on Figure 2 and the mapped physiographic landforms within the Study Area are illustrated on Figure 3.

Based on *Surficial Geology of Southern Ontario*², the surficial geology of the Study Area generally comprises of fine textured glaciolacustrine deposits of silt and clay and interbedded flow till composed of rainout deposits and silt and clay. The mapped surficial geology of the Study Area is illustrated on Figure 4.

¹ Chapman, L.J. and Putnam, D.F. 1984. The Physiography of Southern Ontario, Ontario Geological Survey Special Volume 2, Third Edition. Accompanied by Map P.2715, Scale 1:600,000.

² Ontario Geological Survey, 2010: Surficial geology of Southern Ontario; Ontario Geological Survey, Miscellaneous Release--Data 128-REV



According to *Paleozoic Geology of Southern Ontario*³, the overburden soils are underlain by shale, siltstone, minor limestone and sandstone bedrock of the Queenston Formation. The mapped bedrock geology of the Study Area is illustrated on Figure 5.

The topography on the Site generally slopes down gradually towards the east and the shallow groundwater flow direction is expected to follow topography in a general easterly direction.

2.3 Environmental Setting

Based on a review of Ministry of Natural Resources and Forestry (MNRF) online mapping, natural features within the Study Area include the following:

- A tributary of Spring Creek, which flows generally in a west to east direction, originating at Hansen Road, 100 m north of Eastern Avenue. The tributary crosses Rutherford Road 80 m south of Clark Boulevard. Spring Creek is a tributary of Etobicoke Creek and flows into Etobicoke Creek approximately 650 m south of Courtney Park Drive East and West Service Road. Etobicoke Creek in turn flows into Lake Ontario, approximately 20 km southeast of the Study Area.
- A small wooded area is located around the banks of the tributary of Spring Creek, between Hansen Road and Rutherford Road.

No Areas of Natural Scientific Interest (ANSI) and no wetlands are located in the Study Area.

The mapped natural features within the Study Area are illustrated on Figure 6.

Drainage along Eastern Avenue flows easterly through ditches on both sides of the road to a ditch on the east side of Hansen Road, which in turn flows north to the tributary of Spring Creek 100 m north. The tributary of Spring Creek is channelized from Hansen Road to beyond the Rutherford Road. The creek bed has a concrete block lining through this section as a likely means to protect from erosion.

The Site is located within the Etobicoke Creek watersheds, which is regulated by the Toronto and Region Conservation Authority (TRCA). The Study Area lies within the Toronto Source Water Protection Area (SPA) and partially lies within a Highly Vulnerable Aquifer area (HVA), which is located generally within the north and east halves of the Study Area.

The Site is not located in the designated area of the Oak Ridges Moraine Conservation Act⁴ or the designated area of the Niagara Escarpment Planning and Development Act. In addition, the

³ Armstrong, D.K. and Dodge, J.E.P., 2007: Paleozoic geology of southern Ontario; Ontario Geological Survey, Miscellaneous Release--Data 219.



Site does not lie within any Wellhead Protection Areas (WHPA) or within a Significant Groundwater Recharge Area (SGRA).

Parts of the proposed Clark Boulevard extension between Hansen Road and Rutherford Road are within 30 m of a water body (the tributary of Spring Creek) and the floodplains for the tributary is designated as "Regulated Areas" by the TRCA.

In general, the land use surrounding the current alignment is primarily industrial and commercial properties.

3. INVESTIGATION PROCEDURES

3.1 Subsurface Investigation

The borehole investigation field program was carried out between August 16 and September 23, 2021, and consisted of drilling and sampling a total of twenty five (25) boreholes.

The subsurface stratigraphy encountered in these boreholes generally consisted of pavement structure, topsoil, or mixed fill which was generally underlain by native silty clay to clayey silt or sands and silts soils and sand and silt tills, over shale bedrock. However, the factual data presented on the Record of Borehole sheets takes precedence over this general description and must be used for interpretation of the site conditions. It should be recognized and expected that soil conditions will vary between and beyond borehole locations. A summary of the drilled boreholes details and locations is provided in Table 3-1.

Structure	Approximate Location	Borehole No.	Approx. Ground Elevation (m)	Borehole Termination Depth (m)	Approx. Borehole Termination Elevation (m)
	West Side of Creek – 35 Rutherford Road East Side of Creek – 25 Rutherford Road	BR-01	215.7	8.8 (refusal to augering)	206.9
Clark Boulevard Extension		BR-02	215.4	8.4 (refusal to augering)	207.0
Creek		BR-03	215.2	8.7 (refusal to augering)	206.5
Crossing		BR-04	215.7	9.4 (refusal to augering)	206.2
Clark Boulevard	35 Rutherford Road	CE-01	217.8	3.7	214.1
Extension		CE-02	217.1	3.7	213.4

 Table 3-1: Borehole Details



Structure	Approximate Location	Borehole No.	Approx. Ground Elevation (m)	Borehole Termination Depth (m)	Approx. Borehole Termination Elevation (m)
		CE-03	216.0	3.2	212.8
	25 Rutherford Road	CE-04	215.9	3.7	212.3
	Rutherford	RR-01	215.7	2.1	213.6
	Road	RR-02	215.3	2.1	213.2
		EA-02	223.1	2.1	221.0
		EA-03	222.9	2.9	220.0
	Eastern Avenue	EA-04	222.8	2.9	219.9
		EA-05	222.4	6.7	215.7
		EA-06	222.1	2.1	220.0
		EA-07	221.5	2.9	218.6
		EA-08	220.0	1.8	218.2
Eastern Avenue		EA-09	220.7	2.1	218.5
		EA-10	220.4	2.1	218.2
		EA-11	219.6	2.9	216.7
		EA-12	218.3	1.8	216.5
		EA-13	218.9	2.1	216.8
		EA-014	218.1	4.1	214.0
		EA-15	217.7	2.1	215.5
	Hansen Road	EA-16	217.6	2.1	215.5

The approximate locations of the completed boreholes are shown on the Borehole Location Drawings 30427-1 and 30427-2 in Appendix B.



Groundwater conditions were observed in the open boreholes throughout the drilling operations. Monitoring wells were installed in selected boreholes to permit monitoring of the groundwater levels, conduct hydraulic conductivity testing, and collect ground water samples for chemical analysis. The monitoring wells consisted of 50 mm diameter PVC pipe with a slotted screen sealed at a selected depth within the borehole. The installation details are summarized in Table 3-2.

Borehole No.	Monitoring	Slotted Screen	
	Depth (mbgs)	Elevation (masl)	Length (m)
BR-03	8.5	206.7	1.5
BR-04	9.1	206.6	1.5
EA-05	6.0	216.4	1.5
EA-14	4.0	214.1	1.5

Table 3-2: Monitoring Well Details

Physical laboratory testing of soil samples was carried out at Thurber's laboratory. All recovered soil samples were subjected to visual identification and to natural moisture content determination. Selected samples were also subjected to grain size distribution analysis (hydrometer and/or sieve) and Atterberg Limits testing, where appropriate. Laboratory testing results are summarized on the Record of Borehole sheets included in Appendix A and are presented on the figures included in Appendix C.

3.2 Groundwater Sampling and Chemical Analysis

Groundwater quality samples were collected from selected wells for the purpose of considering disposal options and potential treatment needs at a preliminary level. The results provided in this report are representative of the water sampled from the selected wells at the time of sampling and provide a general understanding of groundwater quality under those conditions; however, the water quality may vary significantly from the results obtained based on location, time, meteorological conditions, and in particular based on construction and dewatering methods. The concentration of suspended solids in the groundwater or in water that is collected during construction dewatering (e.g., from a sump in an open excavation) will significantly affect the concentrations of many regulated parameters, particularly metals. The value of testing groundwater quality during the investigation is primarily to identify the types of potential contaminants that may need to be managed before discharge, the extent to which they are dissolved and therefore unlikely to be filtered by physical means alone, and the presence of



anthropogenic contaminants that are listed in the given discharge criteria that may require specific treatment.

The monitoring wells were developed on October 27, 2021 and November 4, 2021, prior to any sampling or in-situ testing, by purging at least three well volumes. The purpose of purging was to remove excess sediment that may have entered the well during installation, to increase the representativeness of the natural groundwater in the well and to improve the transmissivity of the sand pack and well screen. Development was assessed to be completed based on the number of well volumes purged, stabilization of general chemistry parameters of the pumped groundwater (pH, temperature, conductivity) over time, and qualitative observations such as a decrease in turbidity of the pumped water.

A sample set of unfiltered groundwater and a set of field filtered samples were collected from the monitoring well installed in Boreholes EA-05 using standard sampling techniques (i.e., bailer). The samples were preserved in prepared laboratory sample bottles and stored in a cooler on ice to maintain storage temperatures required by the MECP's *Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act,* as amended (the MECP Analytical Protocols). The samples were submitted to AGAT Laboratories in Mississauga, Ontario for analysis the parameters listed in the Limits of Storm Water Discharge of the Peel Region *Wastewater Bylaw* (No. 53-2010) (the Bylaw) for assessing the potential option of disposing of dewatering discharge.

AGAT is accredited by the Canadian Association for Laboratory Accreditation (CALA) for the testing of the parameters referenced in this report. The analytical methods used by the laboratory are presented in the Certificates of Analysis in Appendix D. The analytical procedures were conducted in accordance with the MECP Analytical Protocols.

A summary of the groundwater samples collected and submitted for chemical analysis is presented in Table 3-3.

Location	Sample IDs	Filtered/ Unfiltered	Type of Chemical Analysis
EA-05	EA-05	Unfiltered	Peel Region Storm Sewer Discharge
EA-05	EA-05F	Field Filtered	Peel Region Storm Sewer Discharge

Table 3-3: Groundwater Samples Submitted for Chemical Analysis



Exceedances of the above standards within the groundwater analytical results are discussed in Section 4.2 and a summary of the exceedances and the laboratory certificates of analysis are included in Appendix D.

3.3 Single Well Response Tests

Rising head single well response tests (slug tests) were carried out on the 50 mm diameter wells installed in Boreholes EA-05, BR-03 and BR-04. The well in Borehole EA-05 is screened in firm to very stiff clayey silt. The majority of the well in Borehole BR-03 is screened in very dense sandy silt till and partially in shale. The well in Borehole BR-04 was screened partially in sandy silt till and partially in shale of the Queenston Formation. A summary of the tests completed, and the depths and screened materials is presented in Section 4.3 and the tests results can be found in Appendix E. The tests were completed using the following method:

- In advance of conducting a slug test, the monitoring well was developed to remove excess sediment and to improve the transmissivity of the sand pack and well screen;
- Once the water level returned to a stabilized level, the static water level was measured and recorded, and a datalogger was inserted into the well approximately 1 cm to 5 cm from the bottom of the well. The datalogger was set to record water levels every 1 to 10 seconds, depending on the anticipated rate of recovery of each well;
- A slug of groundwater was removed from the well to induce a difference in hydraulic head between the well and the surrounding formation (rising head test);
- Manual and electronic measurements of the water level were recorded until the water level in the well recovered sufficiently; and,
- Manual measurements were compared to electronic measurements for quality control of the data.

4. TESTING RESULTS AND ANALYSIS

4.1 Groundwater Level Monitoring

Groundwater levels at monitoring wells were measured manually on October 27, November 04, and November 23, 2021. A summary of the water levels recorded in the monitoring wells is provided in Table 4-1.



Borehole	Date	Measured	Water Level
Dorenole	Date	Depth (mbgs)	Elevation (masl)
	October 27, 2021	1.91	213.27
BR-03	November 4, 2021	1.46	213.73
	November 23, 2021	1.52	213.66
	October 27, 2021	2.24	213.43
BR-04	November 4, 2021	2.09	213.58
	November 23, 2021	2.13	213.54
EA-05	November 4, 2021	1.09	221.33
	November 23, 2021	1.21	221.21
EA-14	November 23, 2021	0.54	217.54

Table 4-1: Measured Groundwater Levels

Notes: mgbs – meters below ground surface

masl – meters above sea level

4.2 Groundwater Quality Results

The groundwater chemical testing results of both the field filtered sample and the unfiltered sample are presented in the laboratory Certificates of Analysis in Appendix D. The groundwater analytical results that exceeded the applicable limits and objectives are presented in the following tables.

Peel Region Wastewater Bylaw

The concentration of the parameters listed in the Bylaw in the groundwater samples collected from Borehole EA-05 were below the Bylaw limits for discharge to storm sewers, except where noted in bold in Table 4-2.



Sample ID	Parameter	Units	Measured Concentration	Storm Sewer Limits
	Fecal Coliform	CFU/100ml	30	0
	Phenols	mg/L	0.090	0.008
	Total Arsenic	mg/L	0.036	0.02
	Total Chromium	mg/L	0.116	0.08
EA-05	Total Copper	mg/L	0.129	0.05
EA-05	Total Manganese	mg/L	4.25	0.05
	Total Nickel	mg/L	0.126	0.08
	Total Phosphorous	mg/L	9.91	0.4
	TSS	mg/L	12400	15
	Total Zinc	mg/L	0.311	0.04
EA-05F	Phenols	mg/L	0.028	0.008
EA-03F	Total Manganese	mg/L	0.169	0.05

 Table 4-2: Groundwater Concentrations Exceeding the Peel Region Bylaw Limits

TSS – Total Suspended Solids

TKN – Total Kjeldahl Nitrogen

The concentrations of several parameters in the unfiltered groundwater sample exceeded the Bylaw limits for discharge to a storm sewer, including the following: Fecal Coliform, Phenols, Total Arsenic, Total Chromium, Total Copper, Total Manganese, Total Nickel, Total Suspended Solids (TSS), and Total Zinc. The concentrations of the parameters which had exceedances in the unfiltered samples were greatly reduced in the field filtered samples however the concentrations of Phenols and Total Manganese also exceeded the Bylaw limits for discharge to a storm sewer.

It is expected that groundwater would require treatment prior to discharge into surface water or any storm sewers. Treatment to remove suspended sediment and associated metals, and possible adjustment of the temperature if discharging to surface water, would likely be the minimum requirements. Additional sampling and testing in comparison to Provincial Water Quality Objectives (PWQOs) will be required if groundwater is to be discharged towards surface water. Where feasible, it is recommended that groundwater should be discharged at least 30 m away from any surface water bodies.

Pre-treatment of dewatering discharge will be the responsibility of the dewatering contractor to ensure that the quality of the dewatering discharge effluent meets applicable discharge criteria. Should the dewatering discharge be contaminated such that the groundwater cannot be treated



to the appropriate water quality criteria, the dewatering contractor shall be responsible for transporting the contaminated groundwater off-site for disposal at an appropriate licensed facility.

4.3 Hydraulic Conductivity

The slug tests were analyzed using the Hvorslev method. The test results indicated that the hydraulic conductivity of the screened formations ranged from 4.6×10^{-9} to 1.9×10^{-6} m/s. Plots of the slug test results are included in Appendix E. The hydraulic conductivity values calculated from the in-situ slug tests are summarized in Table 4-3.

Monitoring Well	Hydraulic Conductivity (m/s)	Screened Formation
EA-05	4.6 x 10 ⁻⁹	Clayey Silt
BR-03	1.9 x 10 ⁻⁶	Sandy Silt Till and Shale
BR-04	1.9 x 10 ⁻⁸	Sandy Silt Till and Shale

 Table 4-3: Single Well Response Test Results

5. DEWATERING ASSESSMENT

Groundwater taking for construction dewatering is governed by the Ontario Water Resources Act (OWRA), Environmental Protection Act (EPA) and the Water Taking and Transfer Regulation 387/04, a regulation under the OWRA. If the water taking rate will be greater than 50,000 L/day and less than 400,000 L/day, then registration on the Environmental Activity and Sector Registry will be required. If the water taking rate will be greater than 400,000 L/day, then a Category 3 Permit to Take Water will be required. On July 1, 2021, changes to EASR registrations came into effect, and storm water values no longer contribute to EASR maximum water taking rates. They are still, however, applicable to maximum water taking rates for PTTWs. A preliminary assessment of the need for water taking permitting is provided herein; however, additional analysis will be required to confirm this.

For the purposes of estimating water taking, the estimated withdrawal rates are conservatively assessed in order to reduce the likelihood that actual pumping rates might exceed the permit allowance thereby stopping work and delaying the Project.

Based on information provided by HDR, it is understood that the structures that may require dewatering include the box culvert crossing structure and channel realignment and any proposed improvements to Eastern Avenue, or the Clark Boulevard Extension, including any utility installations or storm drainage infrastructure. Currently there is only sufficient design information to provide a preliminary dewatering estimate for the box culvert crossing structure and channel realignment. Additional design information will be required to provide a preliminary dewatering



estimate for any of the proposed utility installations or storm drainage infrastructure for Eastern Avenue or the Clark Boulevard Extension. Once engineering drawings for the project, including drawings for structural drainage, any utility installations, and the structure for the creek crossing, are finalized, detailed dewatering estimates should be completed during detailed design, well in advance of construction to support permitting requirements.

The dimensions and conditions that were assumed for the preliminary dewatering assessment are provided in Table 5-1.

Structure	Assumed Excavation Footprint (m)	Lowest Assumed Elevation of Excavation (m)	Assumed Groundwater Elevation (m)	Geologic Units to Dewater
Box culvert crossing structure and channel realignment	60 x 15	213	213.73	Silty clay fill, silt, and silt till, possible sand layers

 Table 5-1: Assumed Excavation Dimensions and Ground Conditions

It is assumed that all excavations would be open cut. The excavation and dewatering methods that will be used in the field will be determined by the selected contractor. The following approach was used to estimate the budgeted peak water taking rate:

- Lowering of groundwater to 1.0 m below the bottom of the excavation, to facilitate a dry, stable work area was assumed.
- A base ground water extraction flow rate was estimated, and a factor of safety of three was applied to this flow rate to provide an allowance for removal of water from storage, variation in hydraulic conductivity, actual excavation dimensions and geometry, and ground water levels due to seasonality or other factors, etc.

The water taking will be temporary in nature (less than one year) for the purpose of construction of the box culvert crossing and channel realignment. Dewatering rates were estimated using the Dupuit analytical solution. A radius of influence for the water taking was also estimated. The radius of influence was calculated using the Sichardt equation. The methods and means of dewatering will be determined by the contractor and its subcontractors.

The calculations and equations for the peak flow rate and radius of influence are provided in Appendix F. The base groundwater flow is estimated to be approximately 19,000 L/day. With a safety factor of three on groundwater flow, the estimated peak flow rate flow is approximately 57,000 L/day. The radius of influence is estimated to extend less than 15 m from the edge of the



excavation. Considering the estimated peak water taking rate is greater than 50,000 L/day, but less than 400,000 L/day, registration on the EASR will be required and will require the preparation of a Water Taking Report and Discharge Report in accordance with the regulations.

It should be noted that at this time no dewatering estimate has been completed for the utility installations or storm drainage infrastructure for Eastern Avenue or the Clark Boulevard Extension, and if additional dewatering is required for those structures, then the above dewatering estimate and permitting requirements may be required to be updated.

Based on our understanding of the geology and water table at the Site, it is anticipated that some dewatering will be required for the construction of any utility installations or storm drainage infrastructure for Eastern Avenue or the Clark Boulevard Extension. Groundwater flow rates through the predominantly native silty clay soils would be low due to the relatively low hydraulic conductivity of that soil. However, water may be perched locally within the sandy fill soils, though it would be of limited volume, and water taking estimates must include rainfall and surface water if they cannot be kept separate from groundwater. Thus, depending on the number and size of the excavations, the need for some form or water taking permit may be required.

The radius of influence from the edge of any excavations for utility installations, drainage infrastructure along Eastern Avenue, and the Clark Boulevard extension, is anticipated to be localized and less than 15 m.

Water that is removed from excavations for dewatering must be discharged or disposed of in accordance with current regulations, whether to the natural environment or to a sewer system. The Water Discharge Plan in the case of an EASR registration or the PTTW and associated Hydrogeological Study will specify conditions on the discharge of the groundwater to the environment.

6. IMPACT ASSESSMENT

Lowering of the shallow groundwater level could potentially reduce the groundwater discharge to nearby natural environmental features and groundwater users, and could potentially result in settlement or ground loss, although the likelihood of significant impacts is low due to the low hydraulic conductivity of the silty clay. Any potential impacts during construction dewatering are expected to be temporary in nature. These potential impacts, however, need to be monitored and managed to minimize impact. At this time, only the impacts in relation to dewatering of the box culvert crossing structure and channel realignment are presented below. During the detailed design, a dewatering assessment should be completed to evaluate the potential need for



construction dewatering for the utility installations or storm drainage infrastructure for Eastern Avenue or the Clark Boulevard Extension and any associated impacts should be assessed.

Potential impacts associated with the construction dewatering may include the following:

Impacts to Surface Water and the Natural Environment

Excavations for the box culvert crossing structure and channel realignment will be located within the Etobicoke Creek watershed and likely be carried out adjacent to the stream channel. Groundwater recharge conditions are likely to exist where flow is generally from channel bed into the subsurface.

The watercourse should be temporarily diverted around excavations during construction if required to keep the excavation dry. Watercourses could be diverted from upstream to the downstream channel using cofferdams and diversion pipes, or equivalent.

Dewatering in the vicinity of a watercourse has some potential to temporarily decrease the surface water flow in the watercourse if excavations are open for extended periods, since the watercourse is within the radius of influence. The effect of the dewatering operations on the surface water flow would be more pronounced at low periods of surface water flow (e.g., in the summer). Considering the dewatering will be temporary in duration and the peak estimated dewatering rate for the creek crossing structure was 57,000 L/day with a radius of influence of less than 10 m, any decrease of flow in the watercourse is anticipated to be negligible.

Groundwater of the quality that was encountered in Borehole EA-05 could not be discharged to the natural environment or a storm sewer without pre-treatment due to exceedances of the Bylaw limits (for storm sewer discharge). Water quality observed during construction will vary from the results obtained during this assessment based on a number of factors. Discharge of groundwater to the natural environment may require approval by the TRCA.

Considering that the proposed extension will occur through an area where manufacturing plants exist, additional groundwater quality sampling will be required at the detailed design phase if the dewatering effluent is to be discharged to the natural environment as per TRCA requirements. The groundwater discharge must meet PWQO if it will be discharged to the natural environment.

Impacts to Groundwater Users

Considering the surrounding study area consists of developed urban land primarily composed of commercial and industrial property use and considering the radius of influence for dewatering for the box culvert crossing structure and channel realignment is less than 10 m, it is not anticipated that domestic well users are within the radius of influence; however, an MECP well record search

Client: HDR File No.: 30427



has not been conducted so this cannot be confirmed at this time. The MECP well record search should be conducted within the radius of influence during detailed design to determine whether a private well survey is warranted.

Geotechnical Impacts

The lowering of groundwater levels can induce ground settlement due to an increase in the effective stress. At the proposed excavations, ground settlements associated with the dewatering activities are anticipated to be minor based on the anticipated groundwater drawdowns discussed in this report; however, an assessment of settlement potential should be completed during detailed design, prior to construction. Also, dewatering through the use of poorly designed wells and extraction systems may draw in silt and sand and cause ground loss.

The low hydraulic conductivity of the silty clay, and the anticipated shallow excavation depths for any utility installations or road widening/construction are not anticipated to result in any ground loss issues. However, an assessment of the settlement potential due to dewatering should be carried out for construction of the bridge or culvert structure for the creek crossing of the Clark Boulevard Extension once final design and locations have been determined.

7. CONCLUSIONS AND RECOMMENDATIONS

7.1 Water Taking Permitting

As discussed in Section 5, the estimated peak water taking rate is greater than 50,000 litres per day but less than 400,000 L/day, based on the preliminary dewatering estimate for the box culvert crossing structure and channel realignment; therefore, registration on the EASR is required and will require the preparation of a Water Taking Report and Discharge Report in accordance with the regulations. It should be noted that at this time no dewatering estimate has been completed for the utility installations or storm drainage infrastructure for Eastern Avenue, or the Clark Boulevard Extension, and if additional dewatering is required for those structures, then the dewatering estimate and permitting requirements may be required to be updated.

Depending on the outcome of further analysis and potentially additional investigation following detailed design, registration on the EASR and preparation of a Water Taking Plan and Water Discharge Plan in the case of peak water taking rates between 50,000 and 400,000 litres per day or application for a Category 3 PTTW and required Hydrogeological Study for water taking rates exceeding 400,000 litres per day, may be required.



The permit application fee from MECP for a Category 3 PTTW is currently \$3,000 and the application will be subject to an administrative review as well as a technical review. MECP may request additional information or testing. The review process typically takes three to five months following submission. The registration fee from MECP for registration of water taking for construction dewatering is currently \$1,190 and no review period is required.

It would be possible to conduct limited construction dewatering without a permit provided the total daily water taking rate is restricted to 50,000 litres per day or less; however, many elements will not be feasible to construct with that limitation, and the rate of construction of feasible elements may be restricted until a water taking permit is obtained.

Additional terms and conditions may apply as determined by the water taking permit process, including performance, monitoring and reporting requirements among others.

7.2 Groundwater Discharge

Water quality observed during construction will vary from the results obtained herein based on a number of factors. An experienced dewatering contractor and water treatment contractor are recommended to be retained to design and operate dewatering and treatment operations as required. Pre-treatment of dewatering discharge would be the responsibility of the contractor to ensure that the quality of the dewatering discharge effluent meets the PWQOs or Peel Region Sewer Use By-Law No. 53-2010 as applicable and determine if more extensive or specific treatment measures are required. Should the dewatering discharge be contaminated such that the groundwater cannot be treated to the appropriate water quality criteria, the contractor would be responsible for managing the water, including potentially storage and further treatment or transporting the contaminated groundwater off-site for disposal at an appropriate licensed facility.

A discharge permit would be required from the Region of Peel to discharge to a Region of Peel sewer. Discharge to the natural environment may require consultation with MECP, and potentially TRCA and MNRF depending on the discharge location.

7.3 Low Impact Development

Silty clay was encountered below the fill soils in most boreholes along Eastern Avenue and along the proposed Clark Boulevard Extension at depths ranging between 0.6 m and 2.2 m and extended to depths of approximately 1.2 m to 3.0 m.

Infiltration rates measured at ground surface were not conducted as part of this investigation but may be required in design depending on the location of infiltration structures. Based on the hydraulic conductivity for the silty clay presented herein, the estimated infiltration rates for the silty



clay are likely to be less than the 15 mm/hour threshold specified in the Stormwater Management Planning and Design Manual, which indicate the Site may not be suitable for implementation of infiltration. Infiltration into the sandy fill that was identified may be feasible if sufficient thickness and separation from the groundwater table can be identified. An appropriate safety factor as specified in the Low Impact Development Stormwater Management Planning and Design Guide should be applied to the estimated infiltration rate when designing infiltration LIDs to account for the natural variation in infiltration rates.

Based on review of the existing site conditions, the designer may elect to modify the proposed bottom elevation of the LID measures. Additional field infiltration tests may be required to confirm the soil infiltration rates at the surface depending on the location of infiltration structures.

Groundwater depths at the Site were typically between 1.5 and 3.0 m, which may limit the effectiveness of infiltration measures.

7.4 Control of Impacts and Monitoring

The following measures are recommended to mitigate the potential for the dewatering activities to cause negative impacts as assessed previously:

- Monitoring of water levels in the monitoring wells prior to, during, and following construction.
- Monitoring of water quality for groundwater collected within the excavation dewatering systems to confirm the water quality is appropriate for the selected discharge option. Monitoring should include visual observations for contamination such as sheen or pure product, as well as for excessive sediment in the discharge, which could be an indication of ground loss.
- Where possible, it is recommended that groundwater should be discharged at least 30 m away from any water bodies including streams.
- If discharge to sewers or surface water bodies is proposed, treatment of groundwater to meet acceptable levels is required. Suitable treatment would likely include measures to address suspended sediment and associated metals and is anticipated to require additional treatment based on findings to date. The operation and monitoring of discharge facilities should be carried out by an experienced dewatering contractor and water treatment contractor familiar with fisheries and water quality requirements.
- Where discharge is to ground surface or water course, temporary erosion control measures should be developed and installed to control erosion at the discharge points. Additional water quality requirements may be imposed by MECP, TRCA and MNRF.



- Long-term impacts will need to be addressed through the implementation of best management practices to help increase the amount of infiltration to the aquifer system and minimize the environmental impacts of the development.
- Installation of clay plugs or similar are recommended for any open cut trenches to limit the preferential movement of groundwater along the trench.

7.5 Future Work

Additional hydrogeological investigation and analysis will be required to support detailed design. The following recommendation are provided based on the findings of the hydrogeological investigations:

- Additional groundwater level monitoring should be conducted to capture further seasonal variation, and additional groundwater sampling may be warranted depending on potential discharge location. Infiltration testing may also be advisable depending on infiltration concepts that may be developed.
- If groundwater is planned to be discharged to surface water, additional groundwater samples should be collected and analyzed in comparison to PWQOs to assess treatment and groundwater disposal options.
- During the detailed design stage, it will be necessary to refine the analysis of the hydrogeological conditions along the Site to estimate the radius of influence and dewatering rates for the utility installations or storm drainage infrastructure for Eastern Avenue or the Clark Boulevard Extension. Based on the detailed design, additional drilling of boreholes and installation of shallow and deep monitoring wells will be required. Consideration should be given to installing monitoring wells approximately 1 m below the proposed depths of excavation. These findings will be used to confirm the water takings requirements and the appropriate approvals from the MECP prior to commencement of construction. They will also assist in determining whether a private well survey is warranted.
- Monitoring wells should be decommissioned in accordance with O. Reg. 903 if they are no longer in use to prevent the creation of vertical conduits for contaminant transport.



8. CLOSURE

We trust that this report provides the information you require at this time. If you have any questions regarding this report, please contact the undersigned at your earliest convenience.

Yours truly,

Thurber Engineering Ltd.



Paul Coulson, P.Geo. Hydrogeologist

Alireza Hejazi, Ph.D., P.Eng. Senior Hydrogeologist

Renato Pasqualoni, P.Eng. Review Engineer/Principal



STATEMENT OF LIMITATIONS AND CONDITIONS

1. STANDARD OF CARE

This Report has been prepared in accordance with generally accepted engineering or environmental consulting practices in the applicable jurisdiction. No other warranty, expressed or implied, is intended or made.

2. COMPLETE REPORT

All documents, records, data and files, whether electronic or otherwise, generated as part of this assignment are a part of the Report, which is of a summary nature and is not intended to stand alone without reference to the instructions given to Thurber by the Client, communications between Thurber and the Client, and any other reports, proposals or documents prepared by Thurber for the Client relative to the specific site described herein, all of which together constitute the Report.

IN ORDER TO PROPERLY UNDERSTAND THE SUGGESTIONS, RECOMMENDATIONS AND OPINIONS EXPRESSED HEREIN, REFERENCE MUST BE MADE TO THE WHOLE OF THE REPORT. THURBER IS NOT RESPONSIBLE FOR USE BY ANY PARTY OF PORTIONS OF THE REPORT WITHOUT REFERENCE TO THE WHOLE REPORT.

3. BASIS OF REPORT

The Report has been prepared for the specific site, development, design objectives and purposes that were described to Thurber by the Client. The applicability and reliability of any of the findings, recommendations, suggestions, or opinions expressed in the Report, subject to the limitations provided herein, are only valid to the extent that the Report expressly addresses proposed development, design objectives and purposes, and then only to the extent that there has been no material alteration to or variation from any of the said descriptions provided to Thurber, unless Thurber is specifically requested by the Client to review and revise the Report in light of such alteration or variation.

4. USE OF THE REPORT

The information and opinions expressed in the Report, or any document forming part of the Report, are for the sole benefit of the Client. NO OTHER PARTY MAY USE OR RELY UPON THE REPORT OR ANY PORTION THEREOF WITHOUT THURBER'S WRITTEN CONSENT AND SUCH USE SHALL BE ON SUCH TERMS AND CONDITIONS AS THURBER MAY EXPRESSLY APPROVE. Ownership in and copyright for the contents of the Report belong to Thurber. Any use which a third party makes of the Report, is the sole responsibility of such third party. Thurber accepts no responsibility whatsoever for damages suffered by any third party resulting from use of the Report without Thurber's express written permission.

5. INTERPRETATION OF THE REPORT

- a) Nature and Exactness of Soil and Contaminant Description: Classification and identification of soils, rocks, geological units, contaminant materials and quantities have been based on investigations performed in accordance with the standards set out in Paragraph 1. Classification and identification of these factors are judgmental in nature. Comprehensive sampling and testing programs implemented with the appropriate equipment by experienced personnel may fail to locate some conditions. All investigations utilizing the standards of Paragraph 1 will involve an inherent risk that some conditions will not be detected and all documents or records summarizing such investigations will be based on assumptions of what exists between the actual points sampled. Actual conditions may vary significantly between the points investigated and the Client and all other persons making use of such documents or records with our express written consent should be aware of this risk and the Report is delivered subject to the express condition that such risk is accepted by the Client and such other persons. Some conditions are subject to change over time and those making use of the Report should be aware of this possibility and understand that the Report only presents the conditions at the sampled points at the time of sampling. If special concerns exist, or the Client has special considerations or requirements, the Client should disclose them so that additional or special investigations may be undertaken which would not otherwise be within the scope of investigations made for the purposes of the Report.
- b) Reliance on Provided Information: The evaluation and conclusions contained in the Report have been prepared on the basis of conditions in evidence at the time of site inspections and on the basis of information provided to Thurber. Thurber has relied in good faith upon representations, information and instructions provided by the Client and others concerning the site. Accordingly, Thurber does not accept responsibility for any deficiency, misstatement or inaccuracy contained in the Report as a result of misstatements, omissions, misrepresentations, or fraudulent acts of the Client or other persons providing information relied on by Thurber. Thurber is entitled to rely on such representations, information and instructions and is not required to carry out investigations to determine the truth or accuracy of such representations, information and instructions.
- c) Design Services: The Report may form part of design and construction documents for information purposes even though it may have been issued prior to final design being completed. Thurber should be retained to review final design, project plans and related documents prior to construction to confirm that they are consistent with the intent of the Report. Any differences that may exist between the Report's recommendations and the final design detailed in the contract documents should be reported to Thurber immediately so that Thurber can address potential conflicts.
- d) Construction Services: During construction Thurber should be retained to provide field reviews. Field reviews consist of performing sufficient and timely observations of encountered conditions in order to confirm and document that the site conditions do not materially differ from those interpreted conditions considered in the preparation of the report. Adequate field reviews are necessary for Thurber to provide letters of assurance, in accordance with the requirements of many regulatory authorities.

6. RELEASE OF POLLUTANTS OR HAZARDOUS SUBSTANCES

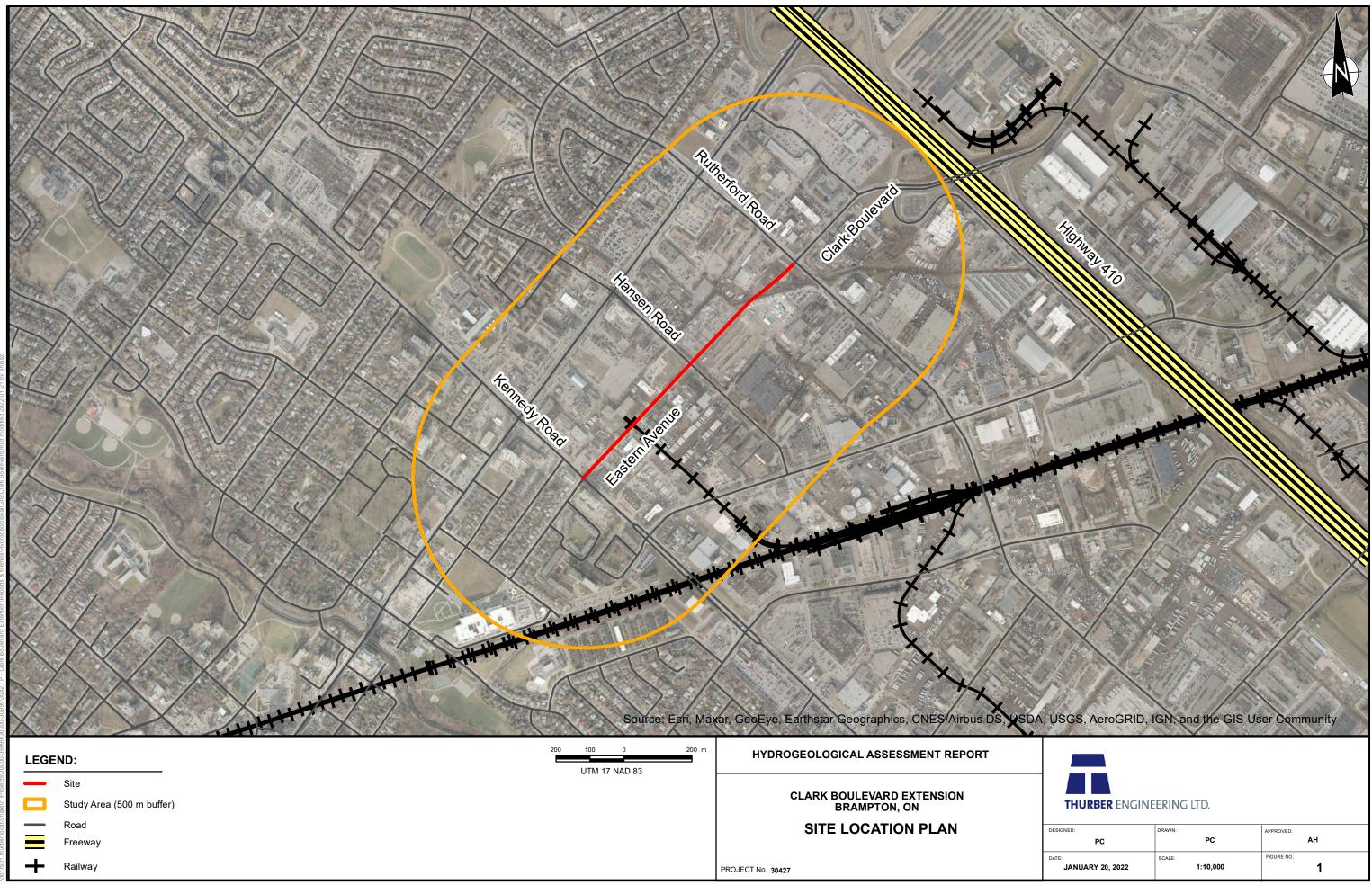
Geotechnical engineering and environmental consulting projects often have the potential to encounter pollutants or hazardous substances and the potential to cause the escape, release or dispersal of those substances. Thurber shall have no liability to the Client under any circumstances, for the escape, release or dispersal of pollutants or hazardous substances, unless such pollutants or hazardous substances have been specifically and accurately identified to Thurber by the Client prior to the commencement of Thurber's professional services.

7. INDEPENDENT JUDGEMENTS OF CLIENT

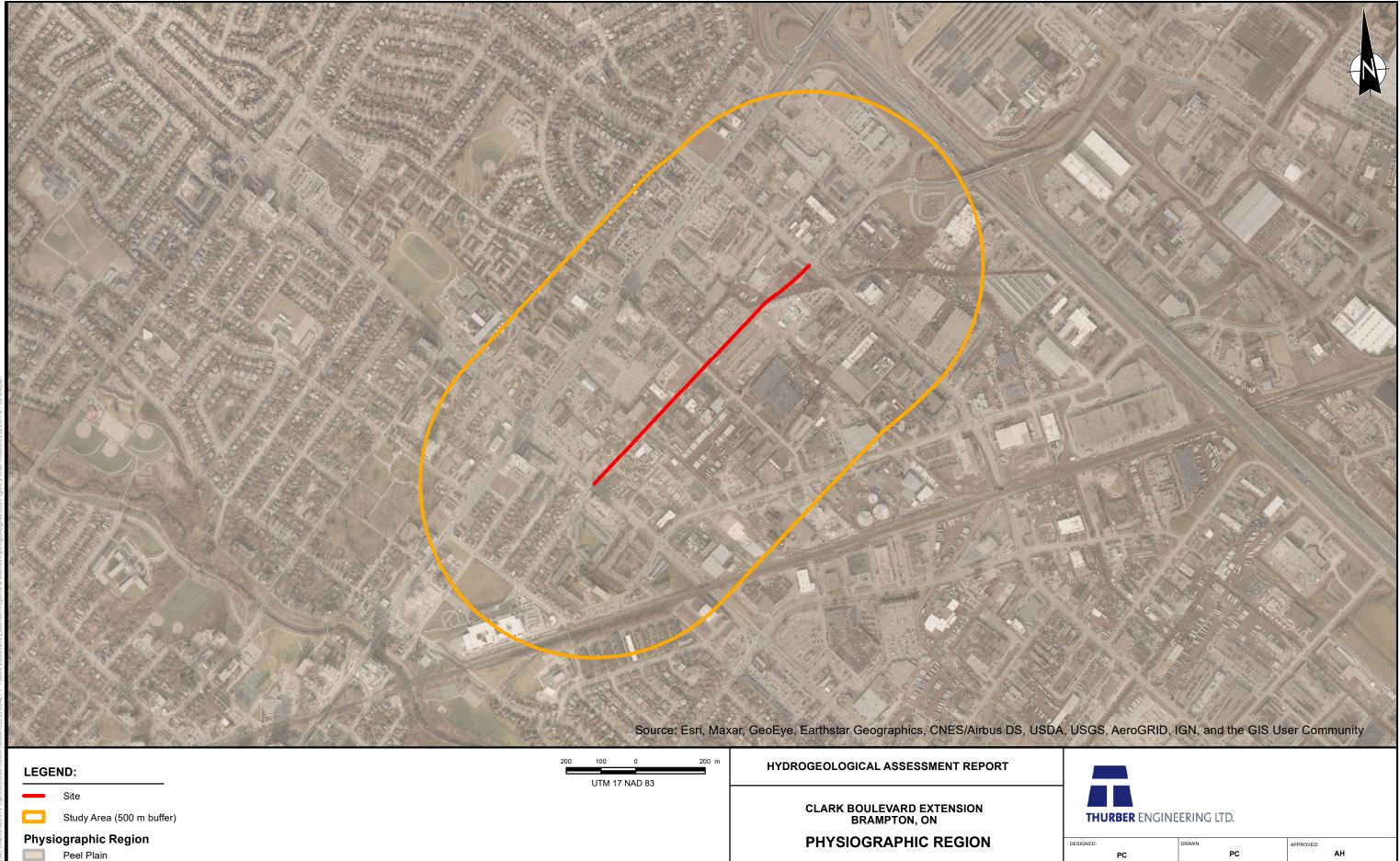
The information, interpretations and conclusions in the Report are based on Thurber's interpretation of conditions revealed through limited investigation conducted within a defined scope of services. Thurber does not accept responsibility for independent conclusions, interpretations, interpretations and/or decisions of the Client, or others who may come into possession of the Report, or any part thereof, which may be based on information contained in the Report. This restriction of liability includes but is not limited to decisions made to develop, purchase or sell land.



Figures



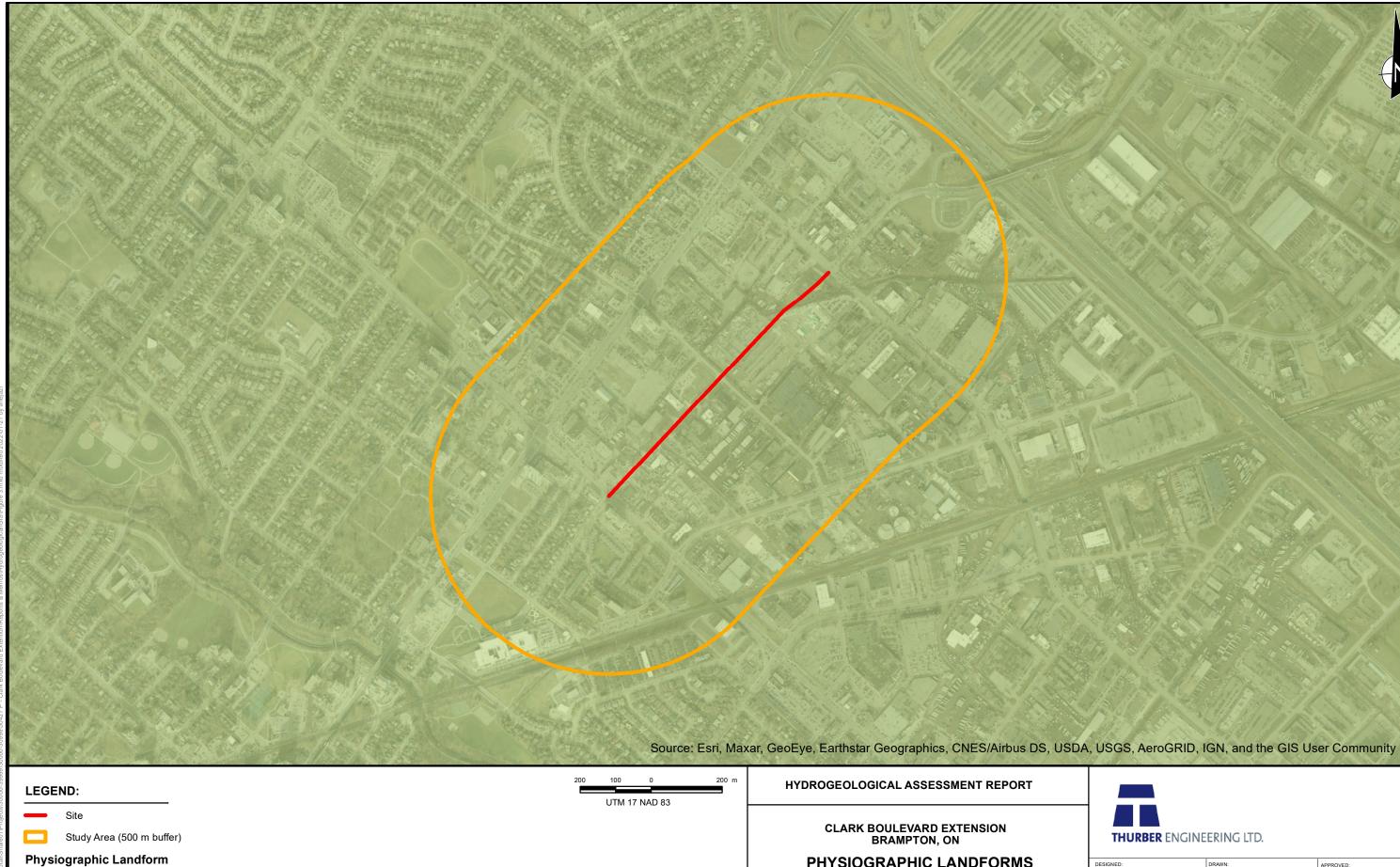
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PHYSIOGRAPHIC LANDFORMS

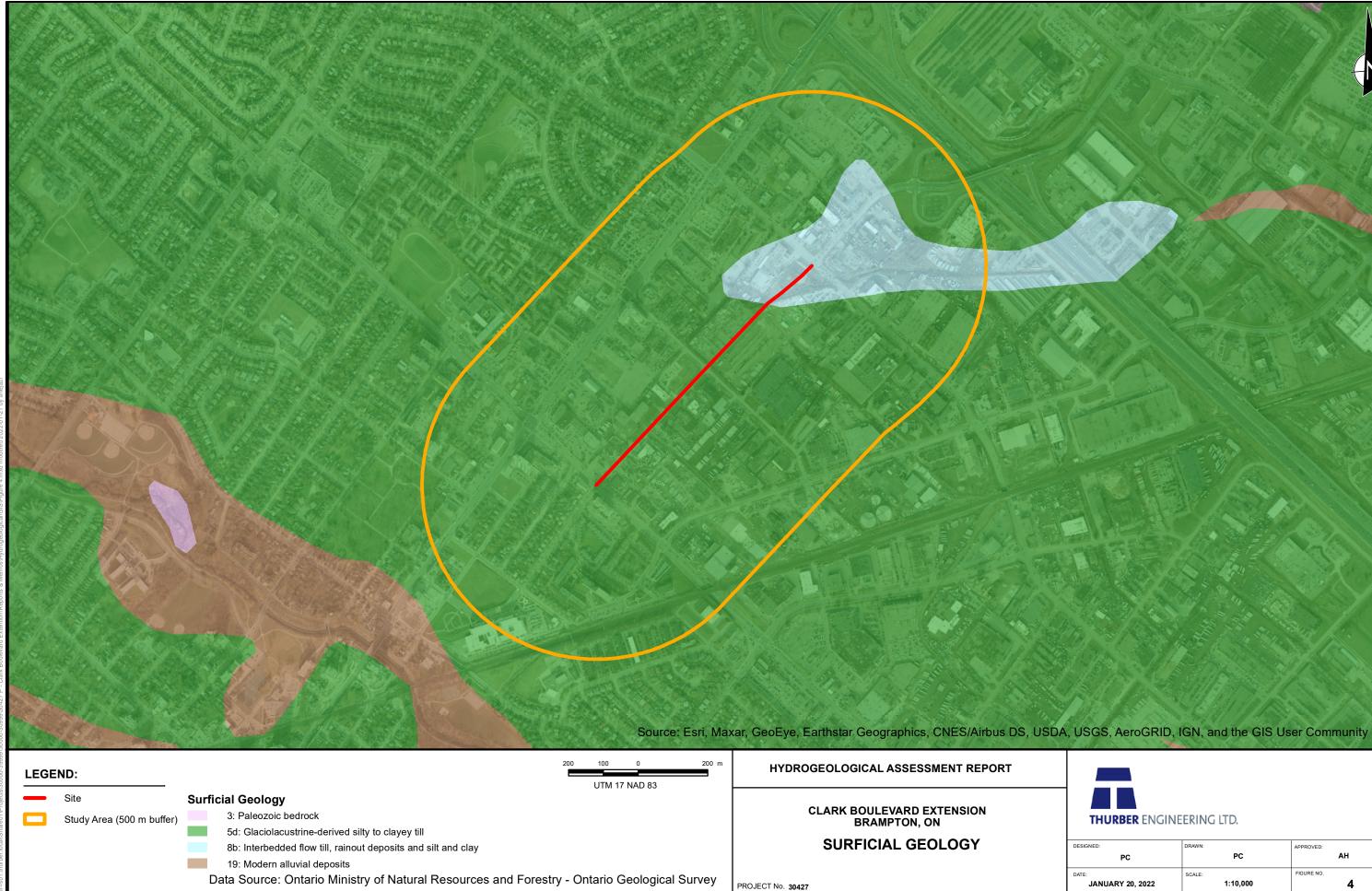
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Bevelled Till Plains

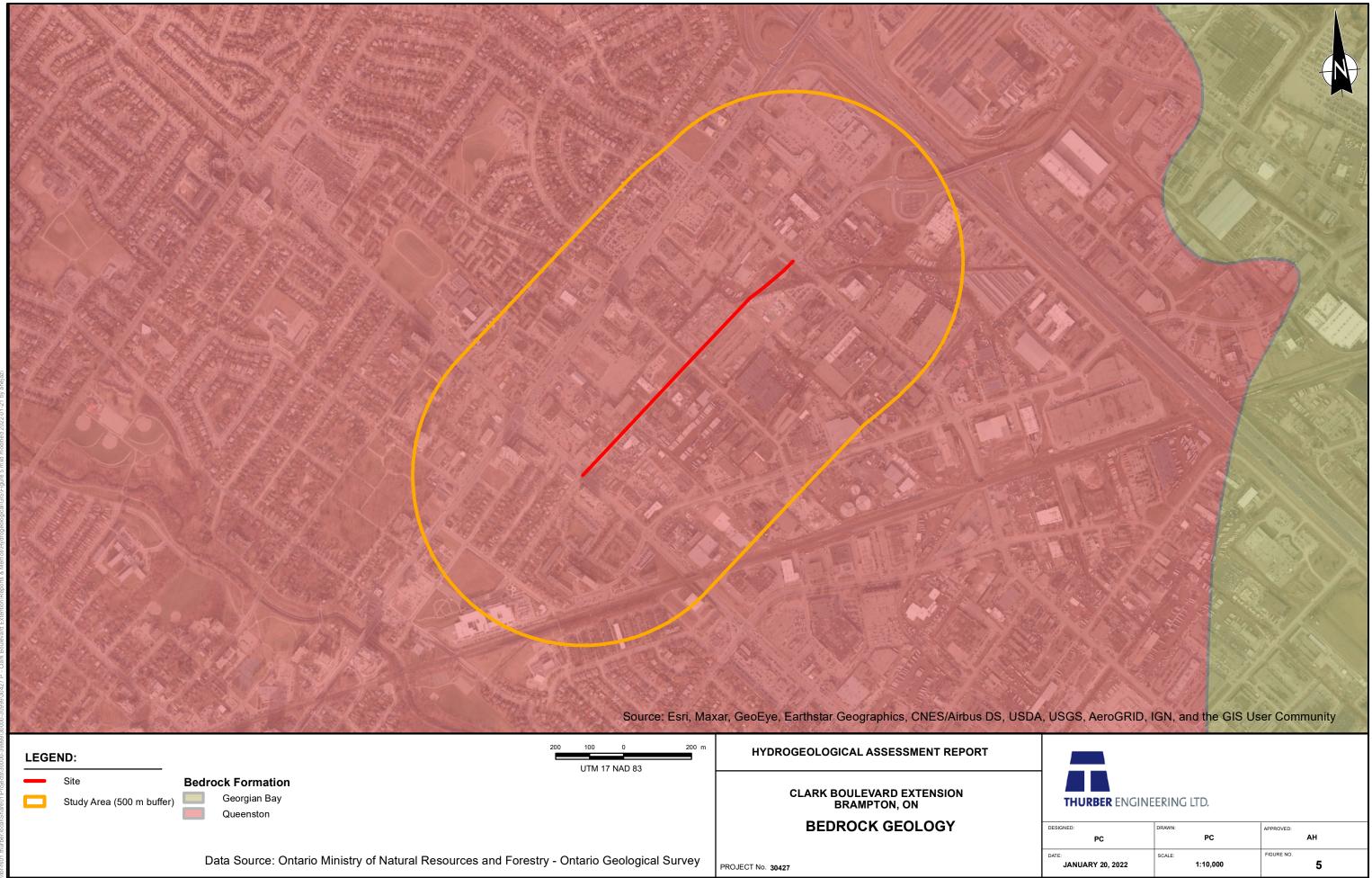
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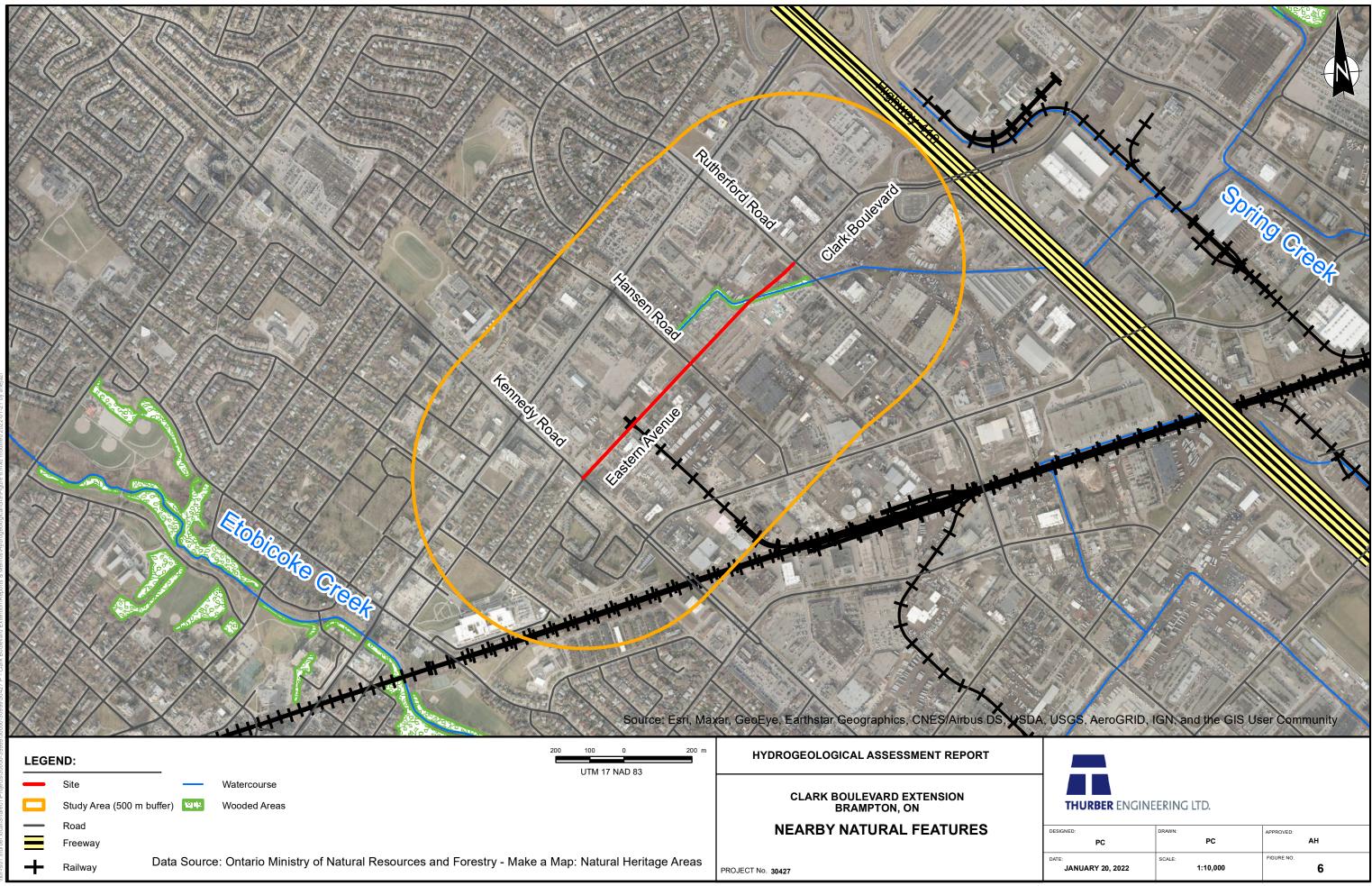
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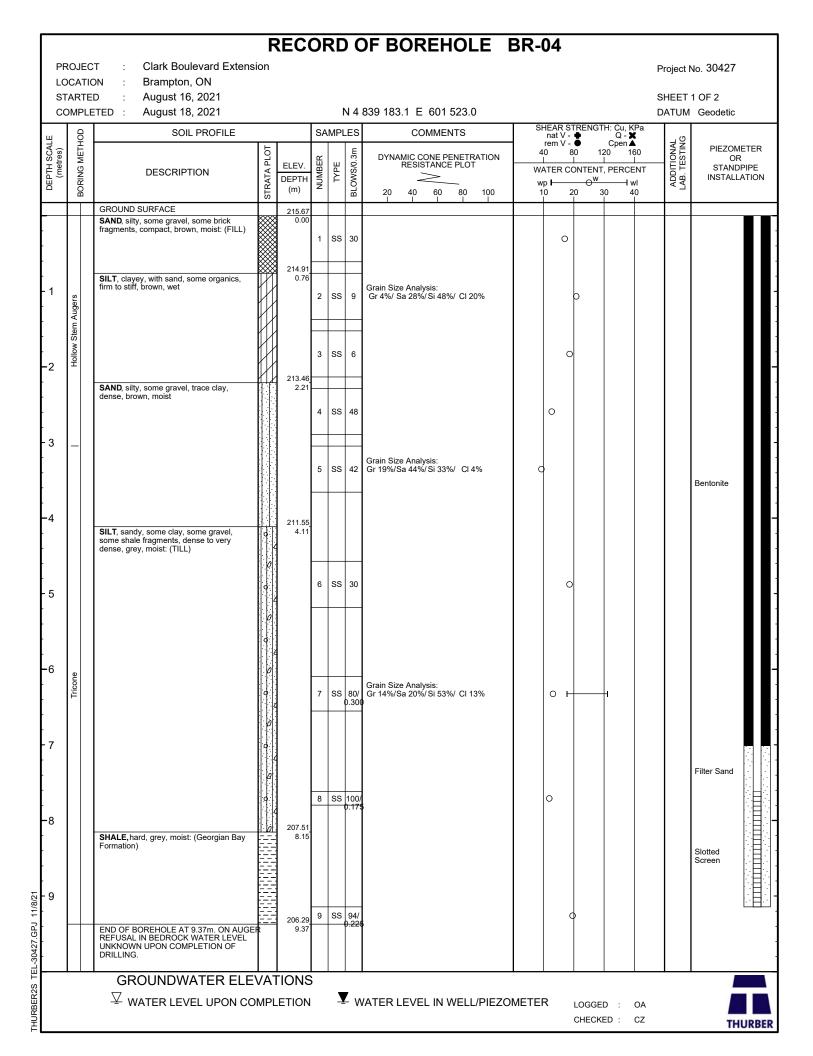
Appendix A

Record of Borehole Sheets

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-		GRAVEL , sandy, some silt, compact, brown, moist: (FILL)		0.00											
ł					1	SS	29		0						
İ.		CLAY, silty, some sand, trace gravel, firm,		215.02 0.69											
- 1		brown, moist: (FILL)			2	SS	6	Grain Size Analysis: Gr 0%/ Sa 20%/ Si 49%/ Cl 31%			×				
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-2				213.50 2.21	—										
ł		SILT, some sand, trace clay, trace gravel, compact, brown, moist		2.21											
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					5	ss	28	Grain Size Analysis: Gr 1%/ Sa 19%/Si 72%/ Cl 8%		0					
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-4	Hollow Stem Augers	SILT, some sand to sandy, trace clay,	-	211.59 4.11											
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ł		dense, grey, moist	۵ ۵												
		END OF BOREHOLE AT 8.81m UPON		206.89	9	SS	100. 0.10		0						
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2		BOREHOLE DRY UPON COMPLETION OF DRILLING. BOREHOLE BACKFILLED WITH													
97.1.5		BENTONITE HOLEPLUG AND GROUT TO SURFACE.													
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		SOIL PROFILE		SÆ			COMMENTS	SHEAR STREN nat V - ♥ rem V - ●	GTH: Cu, KPa Q - 🕱		Geodelic
UEP IN SCALE (metres)	BORING METHOD	DESCRIPTION	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	rem V - ● 40 80 U U U WATER CONTE wp ► ○ 10 20	120 160	ADDITIONAL LAB. TESTING	PIEZOMETEF OR STANDPIPE INSTALLATIO
		GROUND SURFACE SAND, silty, some gravel, trace clay, dense, brown, moist: (FILL)	215.36 0.00	1	ss	35	Grain Size Analysis: Gr 15%/Sa 56%/Si 23%/ Cl 6%	0			
1		CLAY, silty, trace to some sand, trace to some gravel, firm to stiff, dark grey to brown, moist: (FILL)	214.67 0.69		SS	8		0			
2				3	SS	10		0			
		SAND, gravelly, some cobbles, compact, brown, moist	213.07 2.29	4	SS	21		0			
3		SAND and SILT, trace clay, some gravel, some cobbles and boulders, very dense, brown, moist: (TILL)	2.97	5	SS	56	Grain Size Analysis: Gr 13%/Sa 46%/Si 37%/ Cl 4%	0			
4	ow Stem Augers		0								
5	Hollow		Ø	6	SS	50/ 0.15(0			
6			0	7	SS	50/ 0.15(0			
7			0								
8		CLAY, silty, some gravel, highly weathered shale, hard, grey, moist: (TILL)	207.38 7.97 206.98	3	SS			c			Ā
9		END OF BOREHOLE AT 8.38m UPON AUGER REFUSAL ON BEDROCK. WATER LEVEL AT 7.62m UPON COMPLETION OF DRILLING. BOREHOLE BACKFILLED WITH BENTONITE HOLEPLUG AND GROUT TO SURFACE.	<u>206.9</u> € 8.38			0.150					
		GROUNDWATER ELEV					/ATER LEVEL IN WELL/PIEZO				

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		GROUND SURFACE TOPSOIL: (75mm)	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	215.18										
		SAND and GRAVEL compact to dense, brown, moist: (FILL)		0.08	1	ss	19			>				
1	lgers				2	ss	32		0					
2	Hollow Stem Augers	SAND, silty, some gravel, trace clay, compact to very dense, brown, moist		213.71 1.47	3	ss	15	Grain Size Analysis: Gr 16%/Sa 50%/ Si 33%/ Cl 1%		0				
					4	ss	54							
3	_				5	SS	<u>50/</u> 0.10		0					Bentonite
4		SAND and GRAVEL some silt, very dense, grey, moist	* * * * * *	211.32_ 3.86										
5					6	SS	93/ 0.22	5	c					
	Ð	SILT, sandy, some clay, trace gravel, very dense, grey, wet: (TILL)	* * *	209.73 <u></u> 5.45										
6	Tricone		0		7	SS	80/ 0.25							
7			0 0						C					Filter Sand
8		Highly weathered shale fragments	0		8	SS	90/ 0.30	Grain Size Analysis: Gr 6%/ Sa 33%/Si 50%/ Cl 11%		0				Slotted Screen
		SHALE, hard, grey, moist: (Georgian Bay Formation)		206.95 8.23										
9		END OF BOREHOLE AT 8.66m. UPON AUGER REFUSAL ON ASSUMED BEDROCK WATER LEVEL UNKNOWN UPON COMPLETION OF DRILLING. Well installation consists of 50mm diameter Schedule 40 PVC pipe with a 3.05m slotted screen.		206.51 8.66	9	SS	50/ 0.12	5		0				



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DEPTH SCALE (metres)	BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV.	NUMBER	ТҮРЕ	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	WATER CONTENT, PEF	CENT	ADDITIONAL LAB. TESTING	OR STANDPIPE
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щ		Q	SOIL PROFILE			SA	MPI	ES	COMMENTS	SHEAR STRENGTH: Cu, KPa nat V - ● Q - X rem V - ● Cpen ▲	ں _ا	
DEPTH SCALE (metres)		BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	rem V - CpenA 40 80 120 160 I I I 1 WATER CONTENT, PERCENT wp - OW I wI 10 20 30 40	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
-			GROUND SURFACE GRAVEL,sandy, very dense, grey, moist: (FILL)	S S	<u>217.77</u> 0.00	1	SS					
			CLAY, silty, some sand, trace gravel, stiff, grey, moist: (FILL)		217.08 0.69							
- 1	ers				216.24	2	SS	11	Grain Size Analysis: Gr 0%/ Sa 16%/ Si 50%/ Cl 34%	0		
-2	Hollow Stem Augers		CLAY, silty, trace sand, trace gravel, very stiff to hard, brown, moist		1.52	3	ss	17		0		
	Р Ч					4	ss	43		0		
- 3 -			SILT, sandy, some gravel, trace clay, some boulders, dense, grey, moist: (TILL)	0	214.80 2.97		SS	50		0		
-4 -4			END OF BOREHOLE AT 3.66m. BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH BENTONITE HOLEPLUG AND CUTTINGS TO SURFACE.		214.11 3.66							
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THURBER2S TEL-30427.GPJ 11/8/21			GROUNDWATER ELE ☑ WATER LEVEL UPON CC				1	<u> </u>	/ATER LEVEL IN WELL/PIEZC	METER LOGGED : OA CHECKED : CZ		THURBER

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DEPTH SCALE (metres)	BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT		rem V - 40 8 – WATER CC wp – 10 2	0 12 DNTENT	20 160) IT IC	LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
_		GROUND SURFACE	s s	217.06											
-		GRAVEL sandy, compact, brown, moist: (FILL)		0.00	1	ss	22		0						
- - 1 -		SILT, clayey, with sand, trace gravel, hard, brown, moist		0.69	2	ss	23	Grain Size Analysis: Gr 5%/ Sa 31%/Si 42%/ Cl 22%		0					
	Hollow Stem Augers				3	ss	21			0					
-2	Hollow				4	SS	13			0					
- 3															
				213.40	5	SS	35			0					
- 4 -		END OF BOREHOLE AT 3.66m. BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH BENTONITE HOLEPLUG AND CUTTINGS TO SURFACE.		3.66											
- 5															
- - -6															
- 7															
- -8 -															
-															
THURBER2S TEL-30427.GPJ 11/8/21															
EL-3042															
RBER2S TE	<i></i> і	GROUNDWATER ELE ⊈ WATER LEVEL UPON CC				Ţ	<u>v</u>	VATER LEVEL IN WELL/PIEZO	DMET	ER	LOGGEI	D : 0.	A.		
- DH1											CHECKE	ED : C	Z		THURBER

LC ST	DCA FAF	JEC [.] ATIC RTEI	ON : Brampton, ON	sion										_	inaiaat N	00407
ST	STARTED : August 20, 2021 SHEET 1 OF 1 COMPLETED : August 20, 2021 N 4 839 092.3 E 601 410.5 DATUM Geodetic															lo. 30427
		IPLE					1	N 4	839 092.3 E 601 410.5							
ш	(8	SOIL PROFILE			SA	MPL	ES	COMMENTS	5	HEAR S nat V - rem V -		H: Cu, H Q - 🕽			
DEPTH SCALE (metres)		BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	ТҮРЕ	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT 20 40 60 80 100	N N	40 8 /ATER C wp I	30 1 ONTENT 	20 1 	60 ENT	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
	,		GROUND SURFACE	ν. ν	216.03			-						+0		
-			GRAVEL sandy, very dense, brown, moist: (FILL)		0.00	1	ss	60		0						
- - 1 -	jers		SILT, clayey, trace to some sand, trace to some gravel, stiff, brown, moist		0.69		ss	9			0	>				
	Hollow Stem Augers					3	ss	8			0					
-2	Ť		SILT, sandy, some gravel, trace clay, dense to very dense, brown, moist: (TILL)	0	213.83 2.20	4	ss	34	Grain Size Analysis: Gr 19%/Sa 39%/ Si 34%/ Cl 8%		0					
- - 3			300mm dia. boulders at 2.74m Very dense	0	212.83	5	SS	50/		0						
			END OF BOREHOLE AT 3.20m. BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH CUTTINGS TO SURFACE.		3.20			0.150								
-4																
- - 5 -																
- - -6																
- 7																
-8																
THURBER2S TEL-30427.GPJ 11/8/21																
-30427.																
IEL.	L		GROUNDWATER ELE	VA	L FIONS	L		<u> </u>		1	1	<u> </u>		<u> </u>		
THURBER2			abla water level upon CC	DMPL	ETION		Ţ	- w	/ATER LEVEL IN WELL/PIEZC	METE	R	LOGGE CHECK		OA CZ		THURBER

			F	REC	O	RD) (OF BOREHOLE	CE-04		
		ECT : Clark Boulevard Exte TION : Brampton, ON	nsion							Project I	No. 30427
S	TAR	TED : August 16, 2021 PLETED : August 16, 2021				1	۷4	839 225.4 E 601 557.7		SHEET DATUM	1 OF 1 Geodetic
ш	8	-			SA	MPL		COMMENTS	SHEAR STRENGTH: Cu, KPa nat V - ● Q - X rem V - ● Cpen ▲		
DEPTH SCALE (metres)	BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	түре	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT 20 40 60 80 100	rem V - ● Cpen ▲ 40 80 120 160 I I I WATER CONTENT, PERCENT wp I ──── ^W I wl 10 20 30 40	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
		GROUND SURFACE		215.94							
		TOPSOIL: (100mm) SAND, silty, some gravel, some topsoil, compact to loose, brown, moist: (FILL)		0.10	1	ss	20		0		
- 1 - 1	ers	SILT, clayey, some sand, trace gravel, firm, grey, wet		214.95 0.99		ss	5		0		
-2	Hollow Stem Augers				3	ss	5	Grain Size Analysis: Gr 0%/ Sa 17%/ Si 53%/ Cl 30%	0		
	Ĩ			212.97	4	ss	6		0		
- 3		SAND, gravelly, very loose, brown, wet	0 0 0 0 0	2.97	5	ss	3		o		
- -4 -		END OF BOREHOLE AT 3.66m. BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH CUTTINGS TO SURFACE.		3.66							
- 5											
- - -6											
. 7											
-8											
11/8/21 											
THURBER2S TEL-30427.GPJ 11/8/21											
THURBER2S		GROUNDWATER EL				<u> </u>	- v	/ATER LEVEL IN WELL/PIEZC	METER LOGGED : OA CHECKED : CZ		THURBER

State State DESCRIPTION State PERFUSE State<			RE	CO	R) C	F BOREHOLE	EA-02				
STATED ::::::::::::::::::::::::::::::::::::			nsion							P	roject N	lo. 30427
COUNTENT: Solution 15,021 DATUM Countents TOTAL SOLUTION Solution 10,00000000000000000000000000000000000										s	HEET 1	I OF 1
03 03 03 04 <						N 4	838 664.0 E 600 971.2			D		
Sign Display DESCRIPTION Sign Display Display </td <td>ш G</td> <td>SOIL PROFILE</td> <td></td> <td></td> <td>SAM</td> <td>PLES</td> <td>COMMENTS</td> <td>SHEA nat</td> <td>R STRENGTH: CL V - Q</td> <td>i, KPa - 🗙</td> <td>. (7)</td> <td></td>	ш G	SOIL PROFILE			SAM	PLES	COMMENTS	SHEA nat	R STRENGTH: CL V - Q	i, KPa - 🗙	. (7)	
• •	DEP IH SCAL (metres) RING METH	DESCRIPTION	RATA PLOT	LEV. EPTH	NUMBER	OWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	40 	80 120 R CONTENT, PEF	160 I CENT	ADDITIONAL AB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
-1 ABHALT: (100m) - <td></td> <td></td> <td></td> <td>(,</td> <td>2</td> <td>В</td> <td></td> <td>10</td> <td>20 30</td> <td>40</td> <td></td> <td></td>				(,	2	В		10	20 30	40		
1 1 22 1 </td <td></td> <td>ASPHALT: (160mm)</td> <td>22</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		ASPHALT: (160mm)	22									
1 Surf. Taiway, some sand, more gravel. 0 0 0 0 2 3 1 3 10 0 0 3 1 1 1 1 1 0 4 1 1 1 1 1 1 5 1 1 1 1 1 1 6 1 1 1 1 1 1 8 1 1 1 1 1 1	δ	SAND, gravelly, some silt, brown, moist: (GRANULAR BASE)	2	222.45	1 G	s		0				
2 Image: Construct and 2 rates 3 88 21 2 Image: Construct and 2 rates 2 rates 0 3 Image: Construct and 2 rates 2 rates 0 3 Image: Construct and 2 rates 2 rates 0 4 Image: Construct and 2 rates 2 rates 0 5 Image: Construct and 2 rates 1mage: Construct and 2 rates 1mage: Construct and 2 rates 6 Image: Construct and 2 rates Image: Construct and 2 rates 1mage: Construct and 2 rates 7 Image: Construct and 2 rates Image: Construct and 2 rates 1mage: Construct and 2 rates 8 Image: Construct and 2 rates Image: Construct and 2 rates Image: Construct and 2 rates 9 Image: Construct and 2 rates Image: Construct and 2 rates Image: Construct and 2 rates	Stem Auge	SILT, clayey, some sand, trace gravel, very stiff, brown, moist		0.69	2 S	S 15	Grain Size Analysis: Gr 1%/ Sa 20%/Si 51%/ Cl 28%	0				
2: 0 END OF BOREHOLE AT 2 191 DOREHOLE OF UN COMPLETION COMPLETION SUFFACE. 3. 4. 5. 5. 6. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7	Hollow S			-			-					
BORENCE OF AND DRY UPON COMMENTATION SUPPONE	2			221.00	3 S	S 21		0				
		BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH CUTTINGS, THEN ASPHALT TO		2.13								
	3	SURFACE.										
	4											
	5											
	6											
9	7											
9												
	8											
	9											
GROUNDWATER ELEVATIONS WATER LEVEL UPON COMPLETION WATER LEVEL IN WELL/PIEZOMETER LOGGED : AF CHECKED : CZ						Ψv	VATER LEVEL IN WELL/PIEZ	OMETER				THURBER

				R	ECC)R	RD	0	F BOREHOLE	EA-0	3					
		JEC ATIC		ion										F	Project N	lo. 30427
ST	ΓAR	RTEI	2 : September 15, 2021												SHEET	
	-		TED : September 15, 2021 SOIL PROFILE			6.4		N 4	838 683.6 E 601 002.3	SI	HEAR S	TRENG	FH: Cu, K			Geodetic
DEPTH SCALE (metres)		BORING METHOD	SUIL PROFILE	Б				-		4	nat V - rem V - 0 8	. 30 1	FH: Cu, K Q - Cpen 20 1	60	ADDITIONAL LAB. TESTING	PIEZOMETER
EPTH S (metre		M SNIS	DESCRIPTION	STRATA PLOT	ELEV. DEPTH	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT				, PERCE		DDITIC B. TES	OR STANDPIPE INSTALLATION
ä		р В С		STR/	(m)		Ĺ	BLO	20 40 60 80 100		p ┣─── 0 : 	20 :	30 4	VI 40	∠ ¬	
╞──	-		GROUND SURFACE SAND, gravelly, some silt, brown, moist: (FILL)		222.89 0.00											
-						1	GS			0						
İ.			SILT, clayey, trace sand, trace gravel, very stiff, brown, moist: (FILL)		222.20 0.69											
- 1	gers		stiff, brown, moist: (FILL)			2	ss	18			0					
	Hollow Stem Augers				221.44											
-	llow St		SILT, clayey, some sand, trace gravel, very stiff to hard, brown, moist		1.45				Grain Size Analysis: Gr 6%/ Sa 21%/ Si 47%/ Cl 26%							
-2	РH			H]	3	SS	19	Gr 6%/ Sa 21%/Si 47%/ Cl 26%		0					
-						_										
-						4	SS	53			0					
- 3			END OF BOREHOLE AT 2.90m. BOREHOLE OPEN AND DRY UPON	<u>k</u> ly	219.99 2.90											
-			COMPLETION. BOREHOLE BACKFILLED WITH CUTTINGS TO SURFACE.													
-4																
-																
- - 5																
-6																
- - 7																
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-8																
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	_		GROUNDWATER ELE					,								
- 9 - - -			abla water level upon CC	MPL	ETION	I	1	Ľ v	VATER LEVEL IN WELL/PIEZO	OMETEI	R	LOGGE CHECK		AF CZ		
														<u>.</u>		THURBER

				R	ECC)R	D	0	F BOREHOLE	EA-0)4					
				ion										F	Project N	No. 30427
ST	ΓAR	TED					1	N 4	838 703.8 E 601 005.6						HEET	1 OF 1 Geodetic
	-		SOIL PROFILE			SA	MPI			S	HEAR S nat V - rem V -		FH: Cu, P Q - 1			000000
DEPTH SCALE (metres)			DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	W	40 € ⊥ ATER C(/p	30 1 ONTENT 	20 1 	60 ENT	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
_			GROUND SURFACE SAND, some silt and gravel, brown, moist:	***	222.82 0.00											
			(FILL) SILT, clayey, some sand, trace gravel,		222.13 0.69	1	GS			0						
- 1	Hollow Stem Augers		firm, brown, moist: (FILL)		221.37		ss	7	Grain Size Analysis: Gr 0%/ Sa 19%/Si 53%/ Cl 28%		0					
-2	Hollow St		SILT, clayey, some sand, trace gravel, firm to very stiff, brown, moist		1.45	3	ss	8			0					
					219.92		ss	16			0					
- 3			END OF BOREHOLE AT 2.90m. BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH CUTTINGS TO SURFACE.		2.90											
- -4																
- 5																
-																
-6																
- 7																
- - 8																
- 9																
. 12400																
			GROUNDWATER ELE	L VA1	l TIONS	L	<u> </u>			<u> </u>		<u> </u>				
			abla water level upon CC	MPL	ETION		1	Z v	VATER LEVEL IN WELL/PIEZO	OMETE	R	LOGGE CHECK		AF CZ		THURBER

			R	ECC)R	ND	0	F BOREHOLE	EA-05		
			sion							Project I	No. 30427
ST	ARTE	•					N 4	838 728.6 E 601 043.1		SHEET DATUM	1 OF 1 Geodetic
		SOIL PROFILE			SA	MPI		COMMENTS	SHEAR STRENGTH: Cu, KPa nat V - ● Q - X rem V - ● Cpen ▲		-
DEPTH SCALE (metres)	BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	туре	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT		ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
		GROUND SURFACE ASPHALT: (225mm)		222.42 0.00							
		SAND, gravelly, trace silt, brown to grey, moist: (GRANULAR BASE)		0.23		GS		Grain Size Analysis: Gr 35%/Sa 62%/ Si & Cl 3%	0		
		SILT, clayey, some sand, trace gravel, hard to very stiff, brown, wet:		221.71 0.71	2	SS	27		0		
- 1 -			0		3	SS	41		0		
					4	ss	26		0		
-2											Bentonite
-	s		Ø		5	ss	34		0		
-3	Hollow Stem Augers		0		6	ss	15		0		
	Hollow \$		P								
-4 -			0								
		Firm	0		7	ss	7	Grain Size Analysis: Gr 2%/ Sa 22%/Si 47%/ Cl 29%	œ		Filter Sand
- 5 -											Slotted Screen
		Very stiff	0		8	ss	24		o		Screen
-6			0		9	ss	29		0		
- - 7		END OF BOREHOLE AT 6.71m. BOREHOLE OPEN AND DRY UPON COMPLETION.		215.71 6.71							
- -		Well installation consists of 50mm diameter Schedule 40 PVC pipe with a 1.52m slotted screen.									
-8											
-9 -											
- 9		GROUNDWATER ELE					L v	ATER LEVEL IN WELL/PIEZC	DMETER LOGGED : RB CHECKED : CZ		THURBER

			R	ECC)F	RD	0	F BOREHOLE	EA-0	6					
	OJEC		ion										F	Project N	lo. 30427
	CATIO ARTE												c	HEET '	
		ETED : September 15, 2021				I	N 4	838 750.9 E 601 054.9							Geodetic
		SOIL PROFILE			SA	MPI			S	HEAR S	TRENGT	TH: Cu, K Q - X Cpen			
DEP IH SCALE (metres)	BORING METHOD	DESCRIPTION	A PLOT	ELEV.	NUMBER (туре	BLOWS/0.3m		4	3 04	30 1 	20 10	50 	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE
7 7 7	BORIN		STRATA PLOT	DEPTH (m)		≥	BLOW	20 40 60 80 100	w	′p 🛏		v		ADC LAB.	INSTALLATION
	_	GROUND SURFACE ASPHALT: (160mm)		222.09 0.00											
		SAND, gravelly, some silt, brown, moist: (GRANULAR BASE)		0.16	1	GS			0						
		CLAY, silty, trace sand and gravel, very		221.33 0.76											
		stiff to hard, brown, moist:			2	ss	17	Grain Size Analysis: Gr 0%/ Sa 8%/ Si 51%/ Cl 41%		0					
								-							
2				219.95	3	ss	34			0					
		END OF BOREHOLE AT 2.13m. BOREHOLE OPEN AND DRY UPON		2.13				1							
		COMPLETION. BOREHOLE BACKFILLED WITH BENTONITE HOLEPLUG AND CUTTINGS, THEN ASPHALT TO SURFACE.													
					Ĺ										
							7			-					
		abla water level upon co	MPL	-ETION		1	⊢ V	VATER LEVEL IN WELL/PIEZ	JMETE	к	LOGGE CHECK		OA CZ		THURBER

				R	ECC)R	RD	0	F BOREHOLE	EA-0	7					
		JEC		sion										F	Project I	No. 30427
		ATIC RTE												5	SHEET	1 OF 1
C	ОМ	PLE	TED : September 15, 2021					N 4	838 768.1 E 601 086.7						DATUM	Geodetic
ALE		ПОН	SOIL PROFILE			SA	MPL		COMMENTS		HEAR S nat V - rem V -		H: Cu, Q - Cpen	KPa X ▲	NG NG	
DEPTH SCALE (metres)		BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT 20 40 60 80 100	4 W/ w	:0 8 ATER C0	30 1 L ONTENT O^W	20 , PERC	160 ENT	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
_	Ľ		GROUND SURFACE	ە م	221.49											
-			SAND, gravelly, some silt, brown, moist: (FILL)		0.00											
					220.80	1	GS			0						
ŀ			CLAY, silty, trace sand and gravel, firm to stiff, brown, moist: (FILL)		0.69											$\overline{\Delta}$
- 1	ugers	,				2	ss	6			0					
-	Hollow Stem Augers					_										
	ollow S					3	SS	10			0					
-2	Ĭ						33	10								
			CLAY, silty, trace sand and gravel, very stiff, brown, moist		219.28 2.21											
4 SS 15 Grain Size Analysis: Gr 4%/ Sa 31%/Si 45%/ Cl 20% O 218.59 218.59 0 0 0																
- 3	╞		END OF BOREHOLE AT 2.90m.	- #22	218.59 2.90											
ŀ			BOREHOLE OPEN AND WATER LEVEL AT 0.82m UPON COMPLETION. BOREHOLE BACKFILLED WITH													
			CUTTINGS TO SURFACE.													
-																
-4																
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			✓ WATER LEVEL UPON CC September 15, 2021	JMPL	LETION	I	-1	- V	ATER LEVEL IN WELL/PIEZO	JMETE		LOGGE CHECK		AF CZ		
			· ·											-		THURBER

			R	REC	OF	RD) (OF BOREHOLE	EA-08						
	ROJI		nsion								Project I	No. 30427			
		TION : Brampton, ON TED : September 23, 2021									SHEET	1 OF 1			
		PLETED : September 23, 2021				١	۷4	838 792.4 E 601 090.0				Geodetic			
щ	QO	SOIL PROFILE			SA	MPL	ES	COMMENTS	SHEAR STF nat V - I	ENGTH: Cu, KPa Q - X Cpen A	Ч С Г				
DEPTH SCALE (metres)	BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV. DEPTH	NUMBER	түре	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	40 80	120 160 I I NTENT, PERCENT	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION			
B	BOR		STR/	(m)	N		вго	20 40 60 80 100	wp	→ wi 30 40	LA A				
		GROUND SURFACE TOPSOIL: (50mm)		220.02 0.05											
	nood	SAND, silty, some clay, trace gravel, very loose to loose, brown, moist: (FILL)		0.00	1	SS	2		0						
- 1	Continuous Split Spoon				2	SS	6		•						
	Continuo							Grain Size Analysis: Gr 5%/ Sa 48%/ Si 30%/ Cl 17%							
ł				218.19	3	SS	2	Gr 5%/ Sa 48%/Si 30%/ Cl 17%	0						
-2		END OF BOREHOLE AT 1.83m. BOREHOLE BACKFILLED WITH BENTONITE HOLEPLUG TO SURFACE.		1.83					0						
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ŀ															
- 3															
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-4															
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9 - 1															
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(2S IE						_	,		, , ,	4 I					
IUKBEH		abla water level upon C	OMPL	ETION		1	- v	ATER LEVEL IN WELL/PIEZ		OGGED : RB HECKED : CZ					
± 🕒												THURBER			

				R	ECC)R	RD	0	F BOREHOLE	EA-C	9					
		JEC ATIO		ion										F	Project N	lo. 30427
S	TA	RTE	D : September 15, 2021												SHEET ?	
C	-		ETED : September 15, 2021						838 814.3 E 601 129.3	l s	HEAR S	TRENGT	H: Cu. K			Geodetic
s)		BORING METHOD	SOIL PROFILE	5			MPL		COMMENTS		nat V - rem V - 10 8	8 0 1:	TH: Cu, K Q - ¥ Cpen ▲ 20 16	50	NAL TING	PIEZOMETER
DEPTH SCALE (metres)		NG ME	DESCRIPTION	STRATA PLOT	ELEV.	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	w	L ATER C			NT	ADDITIONAL LAB. TESTING	OR STANDPIPE INSTALLATION
DEI		BORI		STRA	DEPTH (m)	NN		BLOV	20 40 60 80 100		/p	20 3	30 4	/I 0	AL	INGTALLATION
_			GROUND SURFACE ASPHALT: (250mm)		220.67 0.00											
-			SAND, gravelly, some silt, brown, moist: (GRANULAR BASE)		0.25	1	GS		Grain Size Analysis: Gr 28%/Sa 50%/ Si 17%/ Cl 5%	0						
ŀ	ders	200	SILT, clayey, some sand, trace gravel,	×	219.98 0.69											
- 1	em Au		stiff, brown, moist			2	ss	10			0					
-	Hollow Stem Augers				219.22											
	E	2	SAND, silty, compact, brown, moist		1.45											
-2						3	SS	17			0					
		+	END OF BOREHOLE AT 2.13m. BOREHOLE OPEN AND DRY UPON	1.1.	218.53 2.13											
-			COMPLETION. BOREHOLE BACKFILLED WITH BENTONITE HOLEPLUG AND CUTTINGS													
- 3			TO SURFACE.													
-																
-4																
- 5																
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											-					
- 9 - - -			abla water level upon CO	MPL	LETION		-1	⊢ V	ATER LEVEL IN WELL/PIEZC	METE	к	LOGGE CHECK		AF CZ		THURBER
																INUKBEK

				R	ECC)F	<u>R</u> D	0	F BOREHOLE	EA-	10					
		JEC		ion										F	Project N	lo. 30427
		ATIC RTE												ç	SHEET '	1 OF 1
			TED : September 15, 2021				I	N 4	838 834.2 E 601 142.4							Geodetic
щ		DO	SOIL PROFILE			SA	MPI	ES	COMMENTS		SHEAR S - nat V - rem V		TH: Cu, K Q - X	(Pa	<u>ں</u>	
DEPTH SCALE (metres)		BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	,	40 8	30 1 L ONTENT O^W	20 1 -, PERCE	60 ENT	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
_	╀		GROUND SURFACE	ν	220.35			ш								
-			ASPHALT: (175mm)		0.00											
ŀ			SAND, gravelly, some silt, brown, moist: (GRANULAR BASE)		0.10	1	GS			0						
ł	ders	5	SILT, clayey, some sand, trace gravel,	Ŵ	219.66 0.69											
- 1	em Al		stiff, brown, moist	K]	2	ss	8	Grain Size Analysis: Gr 2%/ Sa 23%/ Si 47%/ Cl 28%		0					
ŀ	Hollow Stem Augers															
F	모															
•				H		3	ss	10				þ				
-2	┝		END OF BOREHOLE AT 2.13m.	KI.	218.21 2.13											
-			BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH													
İ.			BENTONITE HOLEPLUG AND CUTTINGS TO SURFACE.													
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C	DMF	PLE	TED : September 16, 2021					N 4	838 856.4 E 601 175.1						DATUM	Geodetic
Щ			SOIL PROFILE	.		SA	MPI	LES	COMMENTS	S	HEAR S nat V - rem V -		FH: Cu, k Q - Cpen	(Pa	귀원	
DEPTH SCALE (metres)				STRATA PLOT	ELEV.	ËR	ш	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	4	3 0.	30 1	20 1 	60 I	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE
ш ДЕРТ		- NING	DESCRIPTION	RATA	DEPTH (m)	NUMBER	TYPE	-OWS	\geq	w	р I			wl	ADDI LAB. 1	INSTALLATION
_		ă I	GROUND SURFACE	ST	219.64			B	20 40 60 80 100	1	0 2	20 3	30 4	10		
_			SAND, gravelly, some silt, brown, moist: (FILL)		0.00											
						1	GS			0						
			SILT, clayey, some sand, trace gravel,		218.95 0.69											
1	ş		firm, brown, moist: (FILL)			2	ss	5			0					
	Solid Stem Augers															
	Stem		SILT, clayey, trace sand and gravel, hard, brown, moist	Й	218.19 1.45											
	Solid			H		3	ss	39			0					
-2					217.43											
			SILT , sandy, some clay, some gravel, compact, brown, moist: (TILL)	¢.	2.21				Grain Size Analysis:							
				0		4	SS	28	Grain Size Analysis: Gr 19%/Sa 39%/Si 29%/ Cl 13%		0					
3			END OF BOREHOLE AT 2.90m. BOREHOLE OPEN AND DRY UPON	<u> </u>	216.74 2.90											
			COMPLETION. BOREHOLE BACKFILLED WITH													
			BENTONITE HOLEPLUG AND CUTTINGS TO SURFACE.													
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		ETED : September 23, 2021				I	N 4	838 882.4 E 601 179.4					
щ	B	SOIL PROFILE			SA	MPI	ES	COMMENTS	SHEAF nat	R STRENGT V - 🍨	H: Cu, KPa Q - X Cpen ▲	ں _ا	
DEPTH SCALE (metres)	BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV.	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	40	80 1	20 160 PERCENT		STANDPIPE
DEF	BORI		STRA	DEPTH (m)	R		BLOV	20 40 60 80 100	wp I	20 3		LAE	INSTALLATION
_		GROUND SURFACE TOPSOIL: (25mm)		218.34									
	ing	SAND, some gravel, some silt, very loose, brown, moist: (FILL)	-	0.08	1	ss	1	Grain Size Analysis: Gr 16%/Sa 66%/Si 16%/ Cl 2%	0				
- 1	Continuous Sampling	SILT, clayey, some sand, trace gravel, stiff, brown, moist		0.61		ss	11	Gr 16%/Sa 66%/Si 16%/ Cl 2%					
I	Continuo	SAND, silty, some gravel, trace clay, compact, brown, moist (Till)		217.12 1.22			23						
•		END OF BOREHOLE AT 1.83m.		216.51 1.83		33	23						
-2		BOREHOLE BACKFILLED WITH BENTONITE HOLEPLUG TO SURFACE.											
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State Description State	μ	0	НОР	SOIL PROFILE			SA	MPL	1	COMMENTS		SHEAR STRENGTH: C nat V - C rem V - Cpe	u, KPa ⊧-XX en ∆	귀입	
OPCUME SUFFACE OPCUME	DEPTH SCA (metres)		ORING MET	DESCRIPTION	FRATA PLOT	DEPTH	NUMBER	TYPE	LOWS/0.3m	\geq		40 80 120 WATER CONTENT, PER wp	160 RCENT wl	ADDITION/ LAB. TESTI	OR STANDPIPE
APPARLY: CONTRACT 0.000 0.		-	ā 	GROUND SURFACE	SI		\vdash	-	8				40		
1 Image: State of a state of a						0.00				Crain Size Analysia					
1 0 CMP of BORENQUE AT 2 150. -2 -4	-			SAND and GRAVEL, trace silt, brown, moist: (GRANULAR BASE)		0.25				Gr 30%/Sa 52%/ Si & Cl 18%	0				
2		ugers	,	CLAY silty some sand trace gravel very		218.14 0.76		SS	19						
	1	ow Stem A		stiff to hard, brown, moist				ss	19			0			
-2		Holic Holic													
3 END OF SOCIENCE AT 2 13m 3	-2					216.76		ss	43						
-4 -6 -6 -7 -8 -8 -9 CROUNDWATER ELEVATIONS				BOREHOLE BACKFILLED WITH											
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5 6 7 8 9 CROUNDWATER ELEVATIONS ✓ WATER LEVEL IN WELL/PIEZOMETER LOGGED : 18															
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8 9 GROUNDWATER ELEVATIONS ∑ WATER LEVEL UPON COMPLETION VATER LEVEL IN WELL/PIEZOMETER LOGGED : RB	0														
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9 GROUNDWATER ELEVATIONS ✓ WATER LEVEL UPON COMPLETION ✓ WATER LEVEL IN WELL/PIEZOMETER LOGGED : RB	7														
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ALE	DOH.	SOIL PROFILE		1	SA	MP	-	COMMENTS	s	HEAR S ⁻ nat V - rem V -		H: Cu, ł Q - Cpen	KPa K	RG	DIEZOMETED
DEPTH SCALE (metres)	BORING METHOD		STRATA PLOT	ELEV.	BER	۳ ا	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT		IO 8 L ATER CO	0 1	20 1 	60	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE
DEPT (,	ORIN	DESCRIPTION	FRAT <i>A</i>	DEPTH (m)	NUMBER	ТҮРЕ	LOWS	20 40 60 80 100	. v	′p ——				ADD LAB.	INSTALLATION
		GROUND SURFACE	<u>ک</u>	218.08			-						40		
_		ASPHALT: (200mm)		0.00	1	GS			0						
		SAND and GRAVEL trace silt, compact, brown, moist: (GRANULAR BASE)		0.20											
					2	SS	14		0						Bentonite
1		CLAY, silty, some sand, trace gravel, trace		217.09 0.99		ss	16								
		oxidation, very stiff, mottled brown/grey, moist								0					
	ers														
-2	n Aug				4	ss	15		0						Filter Sand
-2	Hollow Stem Augers	SAND silty gravelly trace clay very		215.87											
	ЫЫ Но	SAND, silty, gravelly, trace clay, very dense, brown, wet: (TILL)	0	4	5		69	Grain Size Analysis: Gr 23%/Sa 43%/ Si 24%/ Cl 10%		0					
			0		5	00	69	GI 23%/Sa 43%/SI 24%/ CI 10%							
3			0												Slotted Screen
			0		6	ss	75			0					Slotted Screen
			0												
-4					7		57/			þ					
•		END OF BOREHOLE AT 4.11m UPON AUGER REFUSAL ON PROBABLE	1.7	213.96 4.11			0.15								
		BEDROCK. Well installation consists of 50mm diameter Schedule 40 PVC pipe with a 1.52m slotted	r												
		screen.	1												
5															
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		GROUNDWATER ELE			L	<u> </u>									
		$\overline{\nabla}$ water level upon co				7	Lν	VATER LEVEL IN WELL/PIEZ	OMETE	R	LOGGE	۰ ח	RB		
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STRETD M. (upuel 18, 2021 SHEET 01 COMPLETED X. Auguel 18, 2021 YA 389 947 9 E 01 2016 SUBARS (EMPTION 100 CONTROL					sion										F	Project N	No. 30427
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Solution Solution	щ	Γ	0	SOIL PROFILE			SA	MPI	ES	COMMENTS	S	HEAR S nat V -		H: Cu, K Q - S	(Pa	ں _ا	
1 A3PHAIT: (200m) 1 8 9 1 Status provide score gray, mont: 0 0.2 1 8 9 1 Status provide score gray, mont: 0 0.2 1 8 9 21 Status provide score gray, mont: 0 0.2 1 8 9 21 Status provide score gray, mont: 0 0.2 1 1 1 0	DEPTH SCAL (metres)		BORING METH	DESCRIPTION	STRATA PLOT	DEPTH	NUMBER	TYPE	BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION						
1 AND green, loss grey, most still, brown, still,	-					217.65 0.00											
-2		y.		SAND, gravelly, loose, grey, moist: (GRANULAR BASE)				ss	9		0	c	>				
-2 -3 3 35 21 -2 -3 -3 -2 -2 -2 -3 -3 -2 -2 -2 -2 -3 -3 -3 -3 -3 -3 -4 -4 -4 -4 -4 -4 -6 -7 -8 -4 -4 -4	- - 1 -	w Stem Auger		SILT, clayey, some sand, trace gravel, stiff, brown, moist			-	SS	14	Grain Size Analysis: Gr 5%/ Sa 26%/Si 46%/ Cl 23%		0					
-100 OF DORENOLE AT 2 300 COMPLETON 2.30 -3 - -3 - -4 - -5 - -6 - -7 - -8 -		Hollo					3	SS	21			0					
-6	-2			BOREHOLE OPEN AND DRY UPON													
				BOREHOLE BACKFILLED WITH CUTTINGS THEN ASPHALT TO													
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9 GROUNDWATER ELEVATIONS ✓ WATER LEVEL UPON COMPLETION WATER LEVEL UPON COMPLETION ✓ WATER LEVEL IN WELL/PIEZOMETER LOGGED : OA	-8																
GROUNDWATER ELEVATIONS ✓ WATER LEVEL UPON COMPLETION ▼ WATER LEVEL IN WELL/PIEZOMETER LOGGED : OA																	
GROUNDWATER ELEVATIONS	-9																
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	┣──			GROUNDWATER ELE	L EVAT	L FIONS	L										
								1	Z v	VATER LEVEL IN WELL/PIEZC	OMETE	R					THURBER

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DEPTH SCALE (metres)		BORING METHOD		STRATA PLOT	ELEV.	ER	ш	0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	4	8 0	30 1	20 16	50	ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE
UEPT OEPT		DRING	DESCRIPTION	RATA	DEPTH	NUMBER	TYPE	BLOWS/0.3m	~	w	р ——		r, PERCE	/I	ADDI LAB. T	INSTALLATION
_		M M	GROUND SURFACE	ST	(m)			BI	20 40 60 80 100	1	0 2	20 3	30 4	0		
			ASPHALT: (275mm)		217.64 0.00											
Ī			SAND, gravelly, compact, brown, moist: (GRANULAR BASE)		217.36 0.28	1	SS	20		0						
	gers		SILT, clayey, with sand, trace gravel, stiff,	- MA	216.95 0.69											
1	em Au		brown, moist			2	ss	12	Grain Size Analysis: Gr 2%/ Sa 30%/ Si 45%/ Cl 23%		0					
	Hollow Stem Augers			H							0					
	오															
~				Н		3	ss	9				þ				
2			END OF BOREHOLE AT 2.13m.	_∦]}	215.50 2.13											
			BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH													
			CUTTINGS THEN ASPHALT TO SURFACE.													
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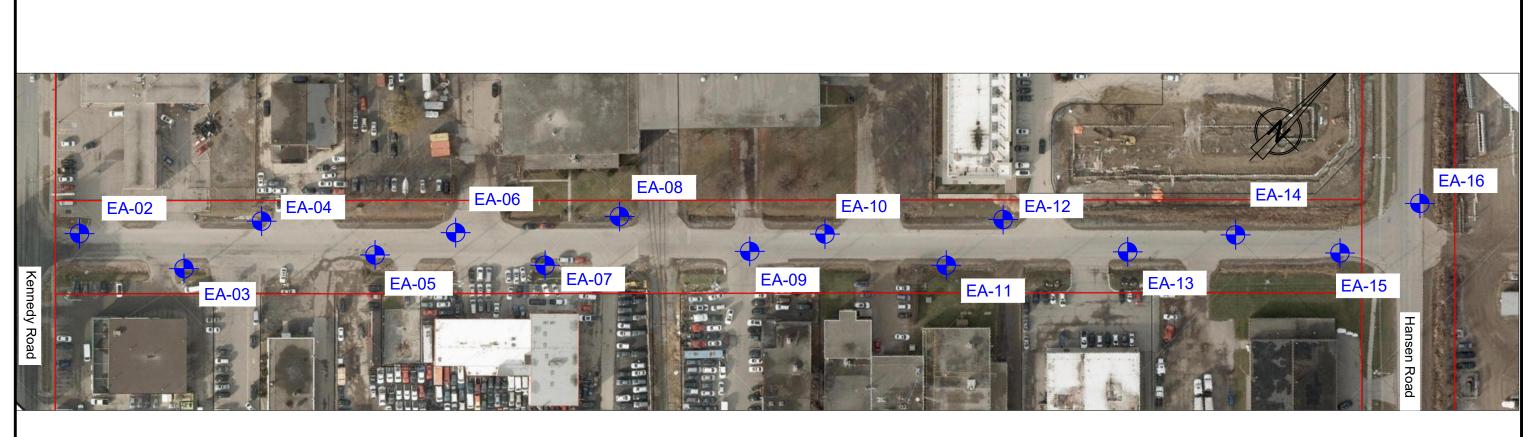
PR					-			OF BOREHOLE							
		CT : Clark Boulevard Extens	sion										Ρ	roject N	lo. 30427
ST	AR	ED : August 18, 2021												HEET	
CC	_	LETED : August 18, 2021						839 278.1 E 601 576.7			TRENGT				Geodetic
) ALE	THOD	SOIL PROFILE	T⊢		SA	MPL		COMMENTS		nat V - rem V -	•	H: Cu, K Q - X Cpen ▲	га	NG NG	PIEZOMETER
DEPTH SCALE (metres)	BORING METHOD	DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	W.	 ATER C(/p 	L ONTENT O ^W	20 16 	ENT /I	ADDITIONAL LAB. TESTING	OR STANDPIPE INSTALLATION
		GROUND SURFACE	ST				В	20 40 60 80 100	1	0 2	20 3	30 4	0		
		ASPHALT: (250mm)		215.69 0.00											
	S	GRAVEL sandy, some asphalt, very dense, brown, moist: (GRANULAR BASE)		0.25		SS	50		0						
- 1	Hollow Stem Augers	SILT, clayey, some sand, trace gravel, stuff, brown, moist		214.93 0.76	2	ss	13	Grain Size Analysis: Gr 2%/ Sa 23%/Si 49%/ Cl 26%		0					
	Hollow														
-2				213.55	3	SS	15						0		
		END OF BOREHOLE AT 2.13m. BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH BENTONITE HOLEPLUG AND CUTTINGS	5.	2.13											
- 3		THEN ASPHALT TO SURFACE.													
-4															
- 5															
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		GROUNDWATER ELE	VA	TIONS	ــــــ ک	1	L		-	1	<u>I</u>	I			
		abla water level upon CC	OMPL	ETION		<u> </u>	<u> </u>	ATER LEVEL IN WELL/PIEZC	OMETE		LOGGE CHECKI		OA CZ		THURBER

				F	REC	0	RD) (OF BOREHOLE	RR-	02					
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ALE (SOIL PROFILE	T ⊢		SA	MPL		COMMENTS	_	nat V - rem V -	•	FH: Cu, K Q - X Cpen ▲	Ра	NG NG	PIEZOMETER
DEPTH SCALE (metres)	BORING METHOD		DESCRIPTION	STRATA PLOT	ELEV.	NUMBER	TYPE	BLOWS/0.3m	DYNAMIC CONE PENETRATION RESISTANCE PLOT	v,	40 i /ATER C wp	80 1 ONTENT 	20 16 	50 L ENT /I	ADDITIONAL LAB. TESTING	OR STANDPIPE INSTALLATION
Ľ			GROUND SURFACE	STI	(m)	<u> </u>		BL			10 :	20 3	30 4	0		
			ASPHALT: (300mm)		215.34 0.00											
-	s		SAND, gravelly, some asphalt fragments, dense, brown, moist: (GRANULAR BASE)		215.03 0.30 214.65	'	SS	47		0						
- 1	n Auger		CLAY , silty, some sand, some gravel, stiff, grey, moist: (FILL)		0.69											
. 1	Hollow Stem Augers					2	SS	9			þ					
	오		SILT, clayey, with sand, trace gravel, stiff, greyish brown, moist	Ŵ	213.81 1.52				Grain Size Analysis: Gr 1%/ Sa 27%/ Si 44%/ Cl 28%							
-2					213.20		SS	12	Gr 1%/ Sa 27%/ Si 44%/ Cl 28%		0					
			END OF BOREHOLE AT 2.13m. BOREHOLE OPEN AND DRY UPON COMPLETION. BOREHOLE BACKFILLED WITH		2.13											
			CUTTINGS, THEN ASPHALT TO SURFACE.													
- 3																
-4																
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i																
			GROUNDWATER ELE	I VA	i Tions	L	<u> </u>					1				
			$\overline{\mathcal{Y}}$ water level upon CC	MPL	ETION		7	Z v	VATER LEVEL IN WELL/PIEZO	ОМЕТЕ	R	LOGGE		OA		
- 9 - -												CHECK	ED :	CZ		THURBER



Appendix B

Borehole Location Plans



Eastern Avenue



GEOTECHNICAL INVESTIGATION

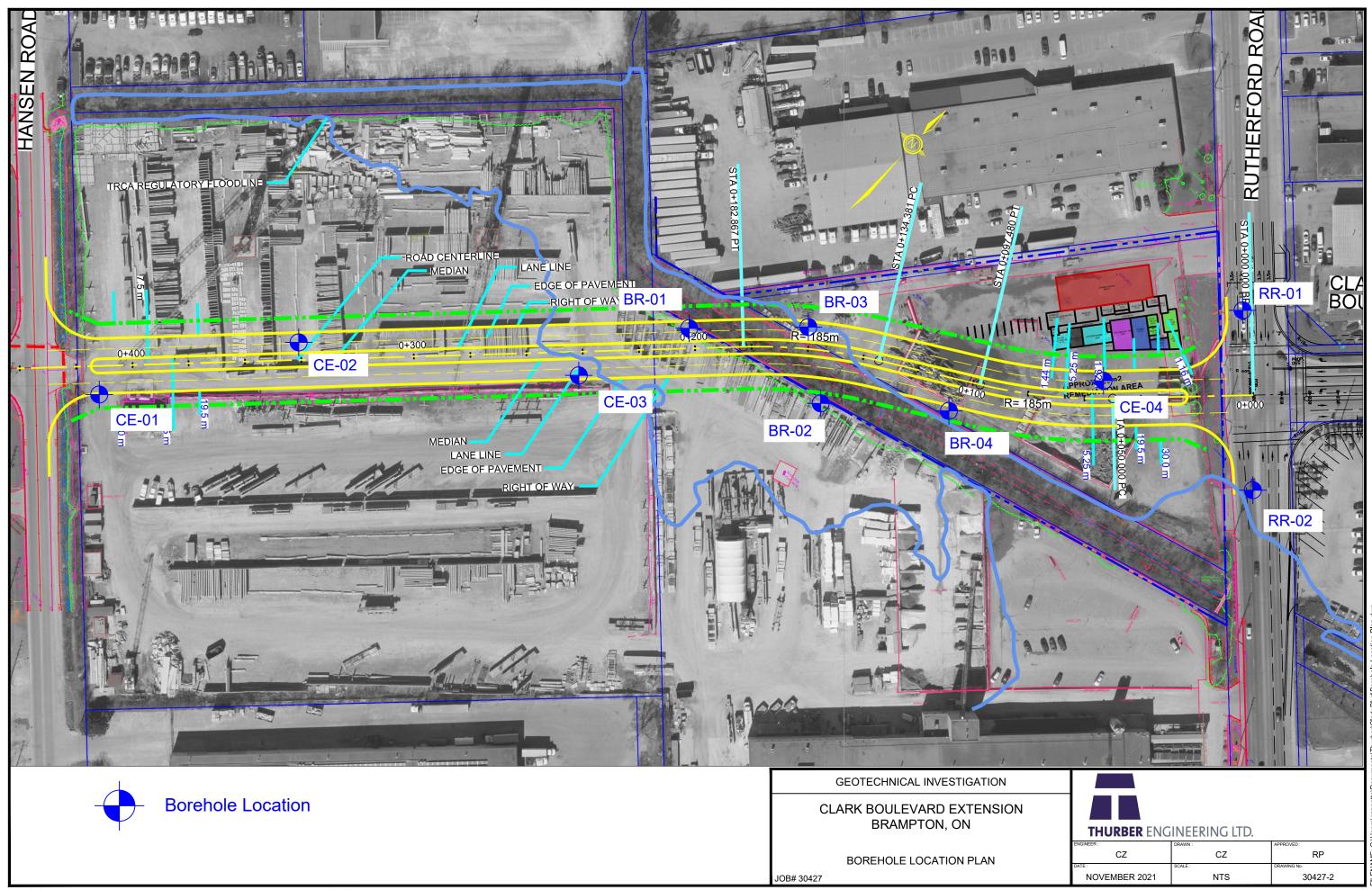
CLARK BOULEVARD EXTENSION BRAMPTON, ON

BOREHOLE LOCATION PLAN

JOB# 30427

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			tonoro
THURBER ENG	INEERING LTD.		VI leare
ENGINEER : CZ	DRAWN : CZ	APPROVED : RP	_
NOVEMBER 2021	SCALE : NTS	DRAWING No. 30427-1	FII FNAMF.

FILENAME: C::Users/czanatta/Documents/Thurber/Clark Blvd/Borehole Location Plan.dwg PLOTDATE: Nov 22, 2021 - 3:08 PM

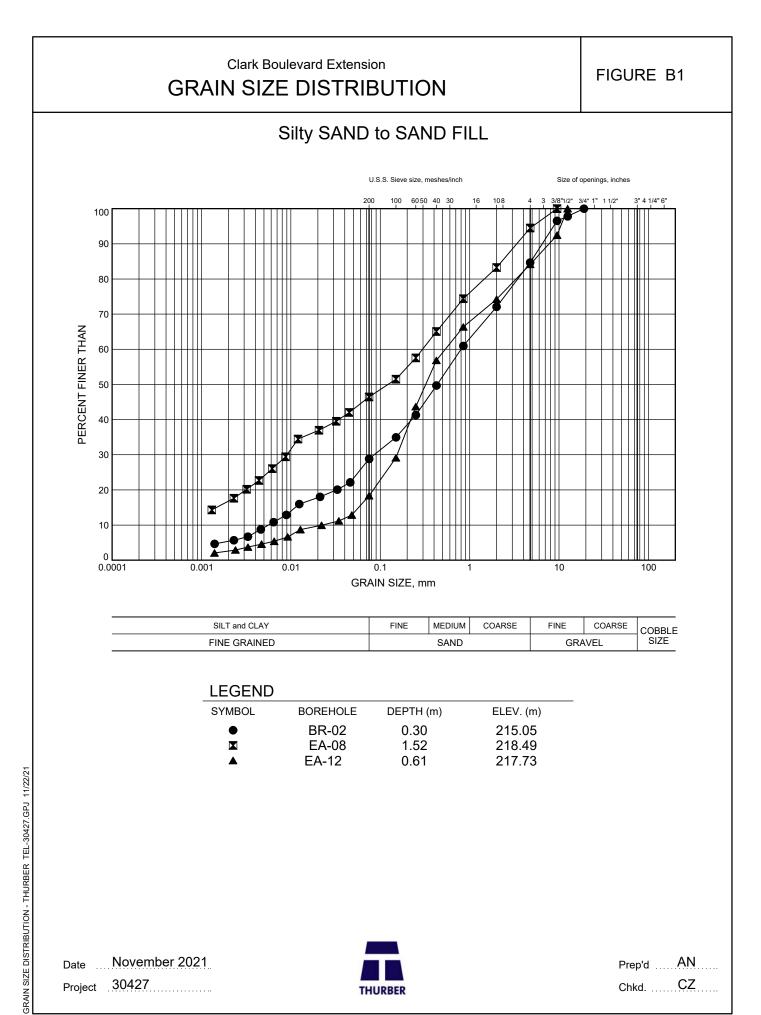


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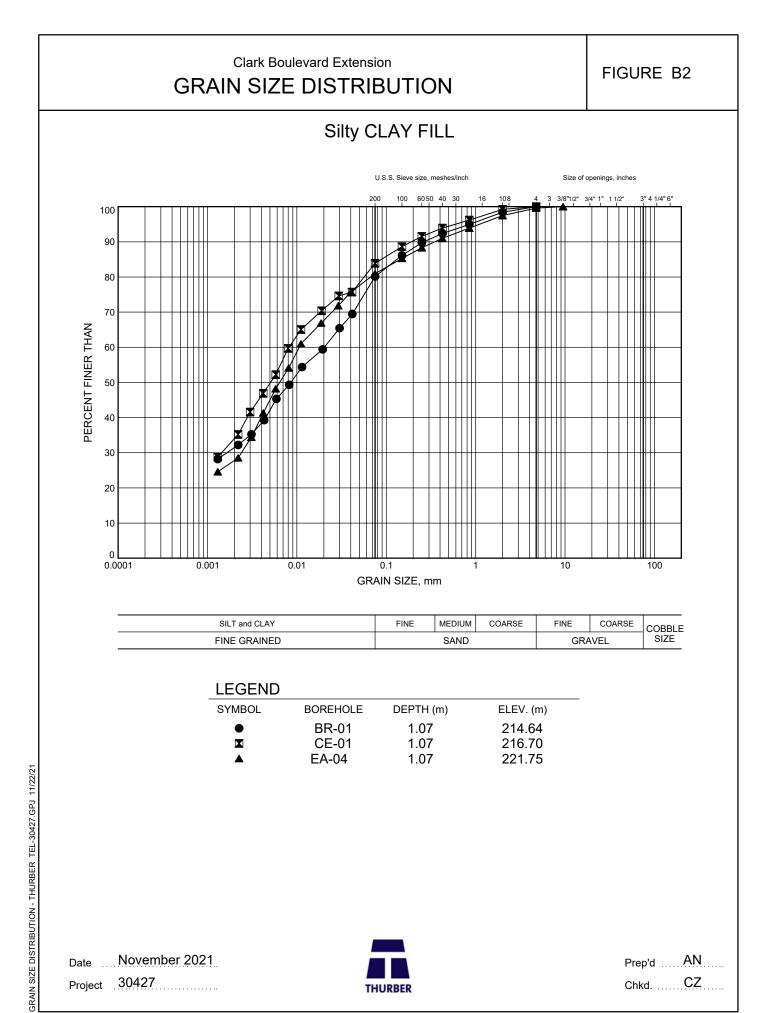


Appendix C

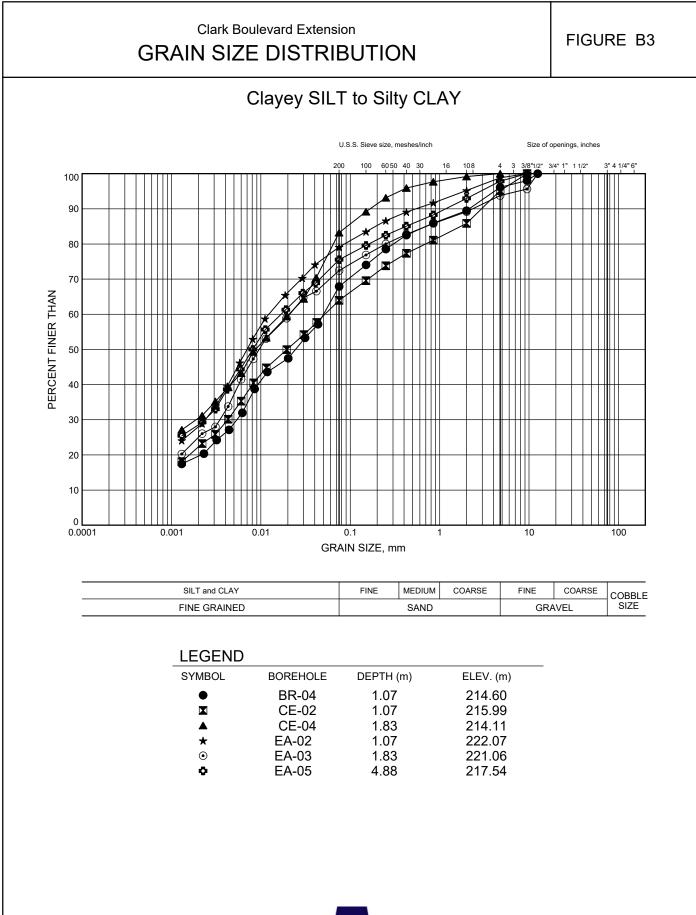
Geotechnical Laboratory Soil Test Results





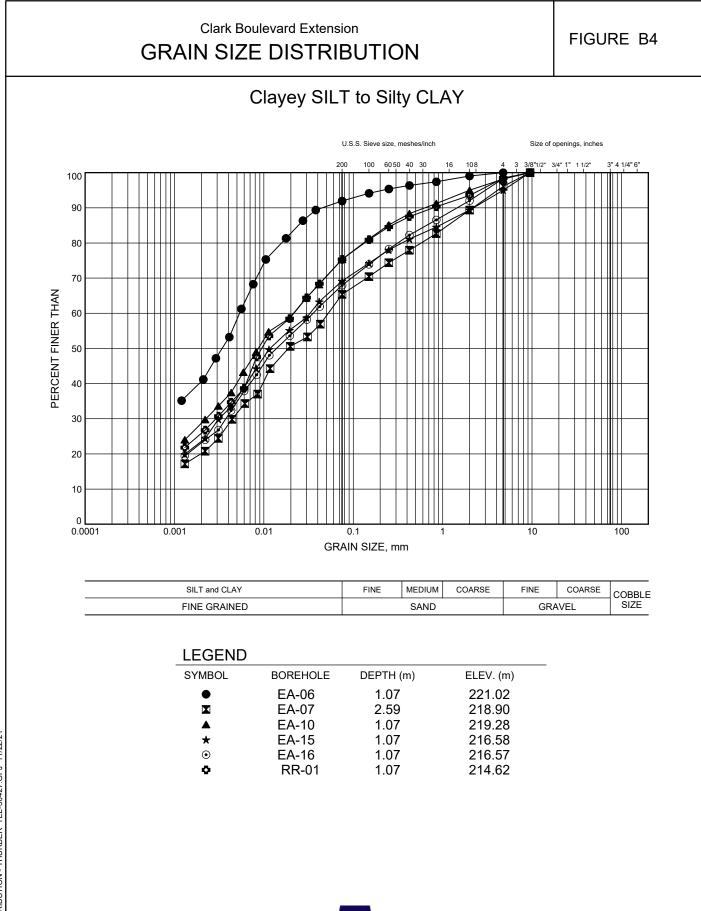






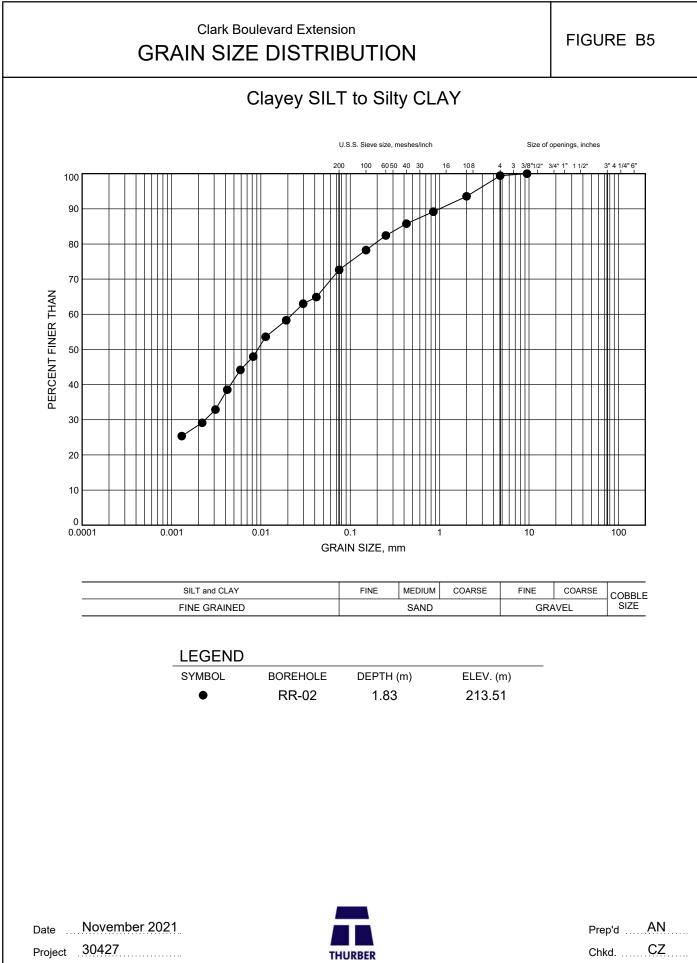
Date November 2021 Project 30427 THURBER

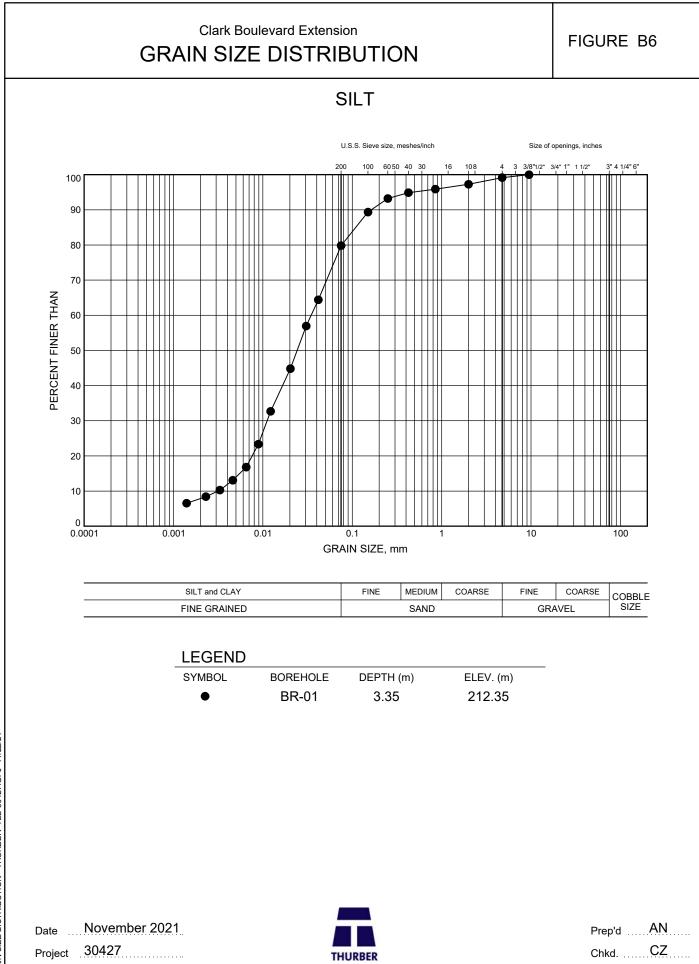
Prep'd AN Chkd. CZ

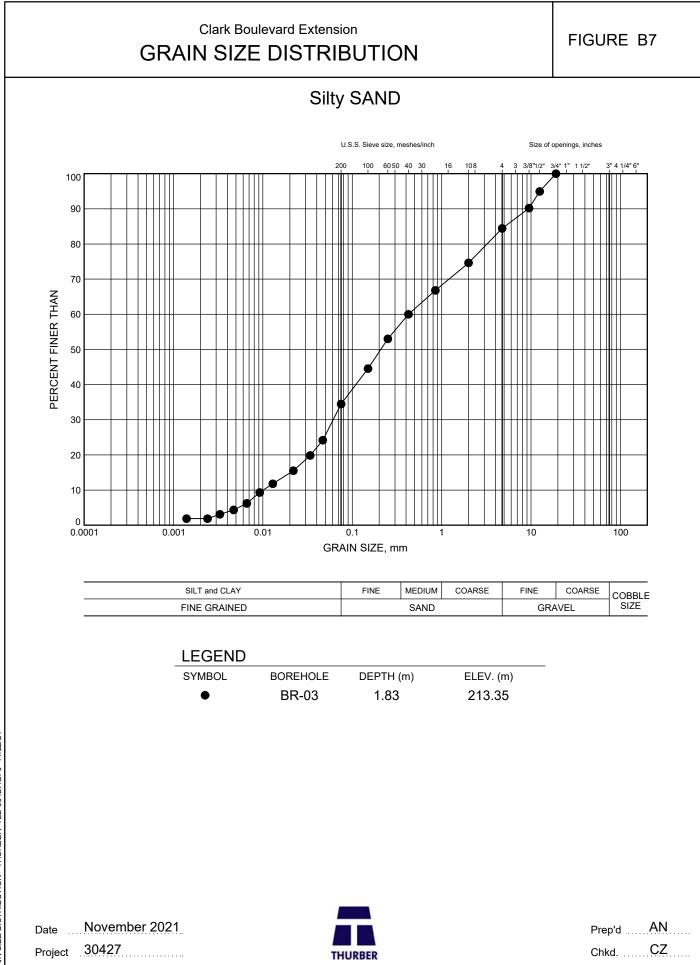


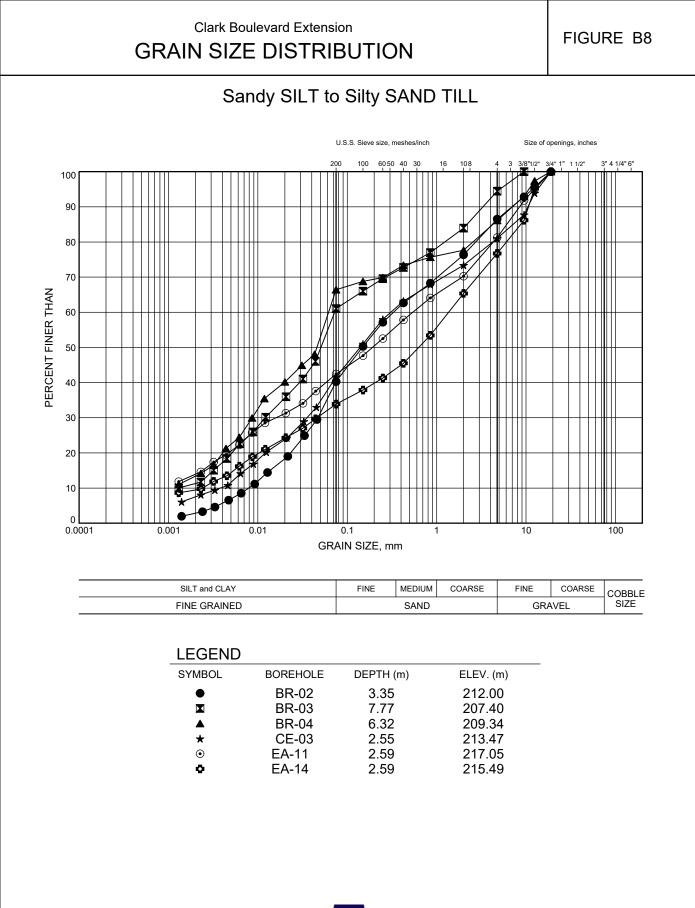
Date November 2021 Project 30427 THURBER

Prep'd AN Chkd. CZ





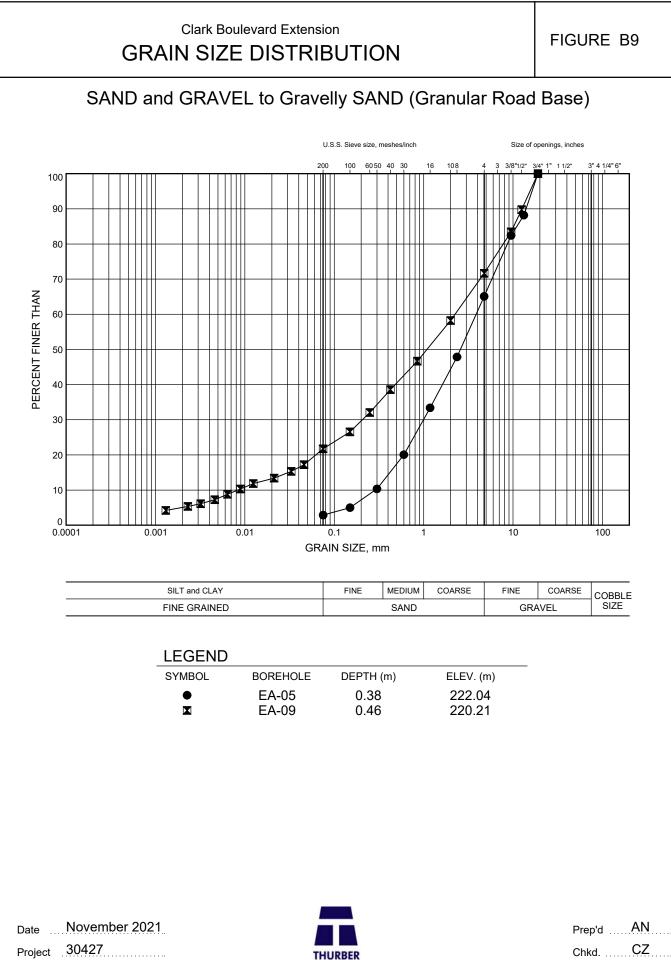




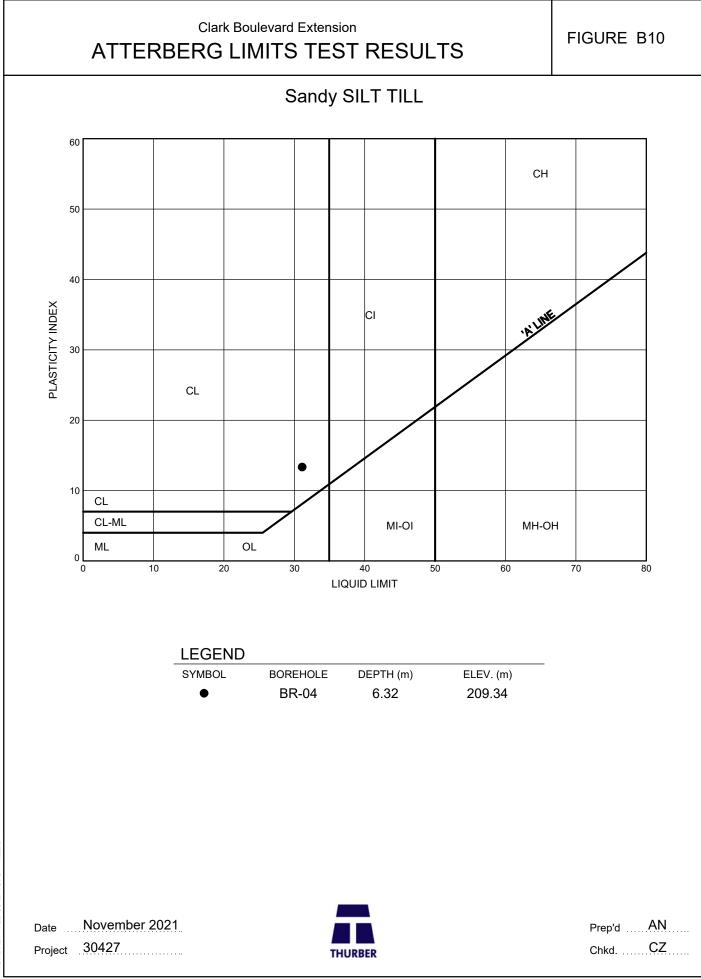
GRAIN SIZE DISTRIBUTION - THURBER TEL-30427.GPJ 11/22/21

Date November 2021 Project 30427 THURBER

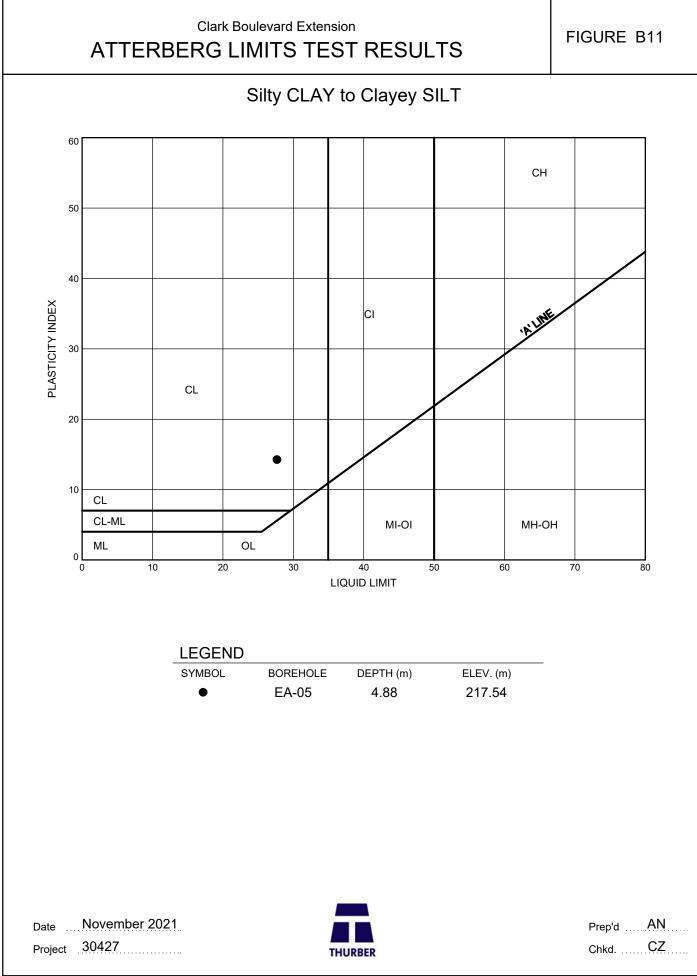
Prep'd AN Chkd. CZ







THURBALT TEL-30427.GPJ 11/22/21



THURBALT TEL-30427.GPJ 11/22/21



Appendix D

Laboratory Certificates of Analysis



CLIENT NAME: THURBER ENGINEERING LTD SUITE 103, 2010 WINSTON PARK DRIVE OAKVILLE, ON L6H5R7 (905) 829-8666 ATTENTION TO: Cary Zanatta PROJECT: 30427 AGAT WORK ORDER: 21T834299 MICROBIOLOGY ANALYSIS REVIEWED BY: Nivine Basily, Inorganics Report Writer TRACE ORGANICS REVIEWED BY: Nivine Basily, Inorganics Lab Supervisor WATER ANALYSIS REVIEWED BY: Vis Verastegui, Report Reviewer DATE REPORTED: Dec 02, 2021 PAGES (INCLUDING COVER): 14 VERSION*: 1

Should you require any information regarding this analysis please contact your client services representative at (905) 712-5100

*Notes

Disclaimer:

- All work conducted herein has been done using accepted standard protocols, and generally accepted practices and methods. AGAT test methods may
 incorporate modifications from the specified reference methods to improve performance.
- All samples will be disposed of within 30 days after receipt unless a Long Term Storage Agreement is signed and returned. Some specialty analysis may be exempt, please contact your Client Project Manager for details.
- AGAT's liability in connection with any delay, performance or non-performance of these services is only to the Client and does not extend to any other third party. Unless expressly agreed otherwise in writing, AGAT's liability is limited to the actual cost of the specific analysis or analyses included in the services.
- This Certificate shall not be reproduced except in full, without the written approval of the laboratory.
- The test results reported herewith relate only to the samples as received by the laboratory.
- Application of guidelines is provided "as is" without warranty of any kind, either expressed or implied, including, but not limited to, warranties of
 merchantability, fitness for a particular purpose, or non-infringement. AGAT assumes no responsibility for any errors or omissions in the guidelines
 contained in this document.
- All reportable information as specified by ISO/IEC 17025:2017 is available from AGAT Laboratories upon request.

AGAT Laboratories (V1)

Iember of: Association of Professional Engineers and Geoscientists of Alberta	
(APEGA)	
Western Enviro-Agricultural Laboratory Association (WEALA)	
Environmental Services Association of Alberta (ESAA)	

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AGAT WORK ORDER: 21T834299 PROJECT: 30427 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com

CLIENT NAME: THURBER ENGINEERING LTD

SAMPLING SITE:

ATTENTION TO: Cary Zanatta

SAMPLED BY:

				E.	Coli (Using	MI Agar)
DATE RECEIVED: 2021-11-24						DATE REPORTED: 2021-12-02
	SA	MPLE DES	CRIPTION:	EA-05	EA-05F	
		SAM	PLE TYPE:	Water	Water	
		DATE	SAMPLED:	2021-11-23	2021-11-23	
Parameter	Unit	G/S	RDL	3245716	3245854	
Escherichia coli	CFU/100mL	200		0	1	

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard: Refers to Peel Storm By-Law 53-2010

Guideline values are for general reference only. The guidelines provided may or may not be relevant for the intended use. Refer directly to the applicable standard for regulatory interpretation.

3245716 Escherichia coli RDL = 10 CFU/100mL. RDL > 1 indicates dilutions of the sample.

The sample was diluted prior to filtration due to the presence of sediments.

3245854 Escherichia coli RDL = 1 CFU/100mL.

Analysis performed at AGAT Toronto (unless marked by *)





AGAT WORK ORDER: 21T834299 PROJECT: 30427 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com

CLIENT NAME: THURBER ENGINEERING LTD

SAMPLING SITE:

ATTENTION TO: Cary Zanatta

SAMPLED BY:

				Fee	cal Coliform	is in Water
DATE RECEIVED: 2021-11-24						DATE REPORTED: 2021-12-02
	SA	MPLE DES	CRIPTION:	EA-05	EA-05F	
		SAM	PLE TYPE:	Water	Water	
		DATE	SAMPLED:	2021-11-23	2021-11-23	
Parameter	Unit	G/S	RDL	3245716	3245854	
Fecal Coliform	CFU/100mL	0		30	0	

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard: Refers to Peel Storm By-Law 53-2010

Guideline values are for general reference only. The guidelines provided may or may not be relevant for the intended use. Refer directly to the applicable standard for regulatory interpretation.

3245716 Fecal Coliforms RDL = 10 CFU/100mL

RDL > 1 indicates dilutions of the sample.

The sample was diluted prior to filtration due to the presence of sediments.

3245854 Fecal Coliforms RDL = 1 CFU/100mL

Analysis performed at AGAT Toronto (unless marked by *)



Certified By:



AGAT WORK ORDER: 21T834299 PROJECT: 30427 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.agatlabs.com

CLIENT NAME: THURBER ENGINEERING LTD

SAMPLING SITE:

ATTENTION TO: Cary Zanatta

SAMPLED BY:

				Peel F	Region Storm	- Organics
DATE RECEIVED: 2021-11-2	4					DATE REPORTED: 2021-12-02
	SA		CRIPTION: PLE TYPE: SAMPLED:	EA-05 Water 2021-11-23	EA-05F Water 2021-11-23	
Parameter	Unit	G/S	RDL	3245716	3245854	
Methylene Chloride	mg/L	0.0052	0.0006	<0.0006	<0.0006	
cis-1,2-Dichloroethylene	mg/L	0.0056	0.0004	< 0.0004	< 0.0004	
Chloroform	mg/L	0.002	0.0004	< 0.0004	<0.0004	
Benzene	mg/L	0.002	0.0004	< 0.0004	< 0.0004	
Trichloroethylene	mg/L	0.008	0.0004	< 0.0004	<0.0004	
Toluene	mg/L	0.002	0.0004	< 0.0004	0.0008	
Tetrachloroethene	mg/L	0.0044	0.0004	<0.0004	<0.0004	
trans-1,3-Dichloropropene	mg/L	0.0056	0.0006	<0.0006	<0.0006	
Ethylbenzene	mg/L	0.002	0.0002	<0.0002	<0.0002	
1,1,2,2-Tetrachloroethane	mg/L	0.017	0.0002	<0.0002	<0.0002	
1,2-Dichlorobenzene	mg/L	0.0056	0.0002	<0.0002	<0.0002	
1,4-Dichlorobenzene	mg/L	0.0068	0.0002	<0.0002	<0.0002	
m & p-Xylene	mg/L		0.0004	< 0.0004	<0.0004	
o-Xylene	mg/L		0.0002	<0.0002	<0.0002	
Xylenes (Total)	mg/L	0.0044	0.0001	<0.0001	<0.0001	
PCBs	mg/L	0.0004	0.0002	<0.0002	<0.0002	
Di-n-butyl phthalate	mg/L	0.015	0.0005	0.0011	0.0015	
Bis(2-Ethylhexyl)phthalate	mg/L	0.0088	0.0005	<0.0005	<0.0005	
Surrogate	Unit	Acceptab	le Limits			
Toluene-d8	% Recovery	50-1	40	98	99	
4-Bromofluorobenzene	% Recovery	50-1	40	98	76	
Decachlorobiphenyl	%	50-1	40	75	89	
2,4,6-Tribromophenol	%	50-1	40	96	89	
2-Fluorophenol	%	50-1	40	93	85	
Chrysene-d12	%	50-1	40	92	94	
phenol-d6 surrogate	%	50-1	40	101	99	

Certified By:

teus



AGAT WORK ORDER: 21T834299 PROJECT: 30427

CLIENT NAME: THURBER ENGINEERING LTD

SAMPLING SITE:

ATTENTION TO: Cary Zanatta

SAMPLED BY:

Peel Region Storm - Organics

DATE RECEIVED: 2021-11-24

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard: Refers to Peel Storm By-Law 53-2010

Guideline values are for general reference only. The guidelines provided may or may not be relevant for the intended use. Refer directly to the applicable standard for regulatory interpretation. 3245716-3245854 Dilution factor=2

The sample was diluted because it was foamy. The reporting detection limit has been corrected for the dilution factor used. Xylenes total is a calculated parameter. The calculated value is the sum of m&p-Xylene and o-Xylene.

Analysis performed at AGAT Toronto (unless marked by *)

Certified By:

DATE REPORTED: 2021-12-02

5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com



AGAT WORK ORDER: 21T834299 PROJECT: 30427 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.aqatlabs.com

CLIENT NAME: THURBER ENGINEERING LTD

SAMPLING SITE:

ATTENTION TO: Cary Zanatta

SAMPLED BY:

					СВО	D5	
DATE RECEIVED: 2021-11-24							DATE REPORTED: 2021-12-02
		SAMPLE DES	CRIPTION:	EA-05		EA-05F	
		SAM	PLE TYPE:	Water		Water	
		DATES	SAMPLED:	2021-11-23		2021-11-23	
Parameter	Unit	G / S	RDL	3245716	RDL	3245854	
Biochemical Oxygen Demand, Carbonaceous	mg/L	15	6.00	<6.00	2.00	3.00	

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard: Refers to Peel Storm By-Law 53-2010

Guideline values are for general reference only. The guidelines provided may or may not be relevant for the intended use. Refer directly to the applicable standard for regulatory interpretation.

3245716 RDL for BOD is raised due to insufficient DO depletion at selected dilution levels.

Analysis performed at AGAT Halifax (unless marked by *)

Certified By:



AGAT WORK ORDER: 21T834299 PROJECT: 30427 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.agatlabs.com

CLIENT NAME: THURBER ENGINEERING LTD

SAMPLING SITE:

ATTENTION TO: Cary Zanatta

SAMPLED BY:

					-	,	5
DATE RECEIVED: 2021-11-24							DATE REPORTED: 2021-12-02
	S	AMPLE DES	CRIPTION:	EA-05		EA-05F	
		SAM	PLE TYPE:	Water		Water	
		DATES	SAMPLED:	2021-11-23		2021-11-23	
Parameter	Unit	G/S	RDL	3245716	RDL	3245854	
рН	pH Units	6.0-9.0	NA	7.89	NA	7.89	
Total Kjeldahl Nitrogen	mg/L	1	0.10	0.77	0.10	0.67	
Phenols	mg/L	0.008	0.008	0.090	0.008	0.028	
Total Phosphorus	mg/L	0.4	1.2	9.91	0.02	0.06	
Total Suspended Solids	mg/L	15	10	12400	10	<10	
Total Cyanide	mg/L	0.02	0.002	<0.002	0.002	<0.002	
Total Arsenic	mg/L	0.02	0.015	0.036	0.015	<0.015	
Total Cadmium	mg/L	0.008	0.001	<0.001	0.001	<0.001	
Total Chromium	mg/L	0.08	0.015	0.116	0.015	<0.015	
Total Copper	mg/L	0.05	0.010	0.129	0.010	<0.010	
Total Lead	mg/L	0.120	0.020	0.042	0.020	<0.020	
Total Manganese	mg/L	0.05	0.020	4.25	0.020	0.169	
Total Mercury	mg/L	0.0004	0.0002	<0.0002	0.0002	<0.0002	
Total Nickel	mg/L	0.08	0.015	0.126	0.015	<0.015	
Total Selenium	mg/L	0.02	0.002	0.003	0.002	0.002	
Total Silver	mg/L	0.12	0.010	<0.010	0.010	<0.010	
Total Zinc	mg/L	0.04	0.020	0.311	0.020	<0.020	
	-						

Peel Storm Sewer Use By-law - Inorganics

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard: Refers to Peel Storm By-Law 53-2010

Guideline values are for general reference only. The guidelines provided may or may not be relevant for the intended use. Refer directly to the applicable standard for regulatory interpretation. 3245716-3245854 Dilution required, RDL has been increased accordingly.

Analysis performed at AGAT Toronto (unless marked by *)

Certified By:

Iris Verastegui



Exceedance Summary

AGAT WORK ORDER: 21T834299 PROJECT: 30427

5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.agatlabs.com

CLIENT NAME: THURBER ENGINEERING LTD

ATTENTION TO: Cary Zanatta

SAMPLEID	SAMPLE TITLE	GUIDELINE	ANALYSIS PACKAGE	PARAMETER	UNIT	GUIDEVALUE	RESULT
3245716	EA-05	ON Peel SM	Fecal Coliforms in Water	Fecal Coliform	CFU/100mL	0	30
3245716	EA-05	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Phenols	mg/L	0.008	0.090
3245716	EA-05	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Total Arsenic	mg/L	0.02	0.036
3245716	EA-05	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Total Chromium	mg/L	0.08	0.116
3245716	EA-05	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Total Copper	mg/L	0.05	0.129
3245716	EA-05	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Total Manganese	mg/L	0.05	4.25
3245716	EA-05	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Total Nickel	mg/L	0.08	0.126
3245716	EA-05	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Total Phosphorus	mg/L	0.4	9.91
3245716	EA-05	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Total Suspended Solids	mg/L	15	12400
3245716	EA-05	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Total Zinc	mg/L	0.04	0.311
3245854	EA-05F	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Phenols	mg/L	0.008	0.028
3245854	EA-05F	ON Peel SM	Peel Storm Sewer Use By-law - Inorganics	Total Manganese	mg/L	0.05	0.169



Quality Assurance

CLIENT NAME: THURBER ENGINEERING LTD

PROJECT: 30427

SAMPLING SITE:

AGAT WORK ORDER: 21T834299

ATTENTION TO: Cary Zanatta

SAMPLED BY:

			Mic	crobi	ology	/ Ana	alysis	5							
RPT Date: Dec 02, 2021			C	UPLICAT	E		REFEREN	NCE MA	TERIAL	METHOD	BLANK	SPIKE	MAT	RIX SPI	KE
PARAMETER	Batch	Sample	Dup #1	Dup #2	RPD	Method Blank	Measured		Acceptable Limits			ptable nits	Recoverv	Lin	eptable nits
		ld	1				Value	Lower	Upper	1 1		Upper		Lower	Upper
E. Coli (Using MI Agar) Escherichia coli	3243507		0	0	NA										
Comments: NA - % RPD Not Applica	able.														
Fecal Coliforms in Water Fecal Coliform	3245716 3	3245716	30	30	0.0%										

Certified By:



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Quality Assurance

CLIENT NAME: THURBER ENGINEERING LTD

PROJECT: 30427

SAMPLING SITE:

AGAT WORK ORDER: 21T834299 ATTENTION TO: Cary Zanatta

SAMPLED BY:

Trace Organics Analysis

					5		,, ,																
RPT Date: Dec 02, 2021			C	UPLICAT	E		REFERE	NCE MA	TERIAL	METHOD	BLANK	SPIKE	MAT	RIX SPI	KE								
PARAMETER	Batch	Sample	Dup #1	Dup #2	RPD	Method Blank	Measured Value	/leasured Lim		Acceptable d Limits		sured Limits		easured Limits				Recovery	1 1 1 1	eptable nits	Recovery	Lie	eptable mits
							Value	Lower	Upper		Lower	Upper		Lower	Upper								
Peel Region Storm - Organics																							
Methylene Chloride	3251511		<0.0003	<0.0003	NA	< 0.0003	95%	50%	140%	98%	60%	130%	110%	50%	140%								
cis-1,2-Dichloroethylene	3251511		<0.0002	<0.0002	NA	< 0.0002	114%	50%	140%	95%	60%	130%	81%	50%	140%								
Chloroform	3251511		<0.0002	<0.0002	NA	< 0.0002	115%	50%	140%	113%	60%	130%	86%	50%	140%								
Benzene	3251511		<0.0002	<0.0002	NA	< 0.0002	83%	50%	140%	82%	60%	130%	87%	50%	140%								
Trichloroethylene	3251511		<0.0002	<0.0002	NA	< 0.0002	117%	50%	140%	104%	60%	130%	84%	50%	140%								
Toluene	3251511		0.0005	0.0005	NA	< 0.0002	116%	50%	140%	96%	60%	130%	50%	50%	140%								
Tetrachloroethene	3251511		<0.0002	<0.0002	NA	< 0.0002	83%	50%	140%	105%	60%	130%	109%	50%	140%								
trans-1,3-Dichloropropene	3251511		<0.0003	<0.0003	NA	< 0.0003	109%	50%	140%	109%	60%	130%	104%	50%	140%								
Ethylbenzene	3251511		<0.0001	<0.0001	NA	< 0.0001	73%	50%	140%	102%	60%	130%	83%	50%	140%								
1,1,2,2-Tetrachloroethane	3251511		<0.0001	<0.0001	NA	< 0.0001	113%	50%	140%	116%	60%	130%	114%	50%	140%								
1,2-Dichlorobenzene	3251511		<0.0001	<0.0001	NA	< 0.0001	83%	50%	140%	97%	60%	130%	85%	50%	140%								
1,4-Dichlorobenzene	3251511		<0.0001	<0.0001	NA	< 0.0001	86%	50%	140%	95%	60%	130%	90%	50%	140%								
m & p-Xylene	3251511		<0.0002	<0.0002	NA	< 0.0002	100%	50%	140%	105%	60%	130%	88%	50%	140%								
o-Xylene	3251511		<0.0001	<0.0001	NA	< 0.0001	75%	50%	140%	102%	60%	130%	87%	50%	140%								
PCBs	3245309		< 0.0002	< 0.0002	NA	< 0.0002	103%	50%	140%	84%	50%	140%	77%	50%	140%								
Di-n-butyl phthalate	3254493		< 0.0005	< 0.0005	NA	< 0.0005	78%	50%	140%	90%	50%	140%	106%	50%	140%								
Bis(2-Ethylhexyl)phthalate	3254493		< 0.0005	< 0.0005	NA	< 0.0005	85%	50%	140%	98%	50%	140%	95%	50%	140%								

Comments: When the average of the sample and duplicate results is less than 5x the RDL, the Relative Percent Difference (RPD) will be indicated as Not Applicable (NA).

Certified By:

wg

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Quality Assurance

CLIENT NAME: THURBER ENGINEERING LTD

PROJECT: 30427

SAMPLING SITE:

AGAT WORK ORDER: 21T834299

ATTENTION TO: Cary Zanatta

SAMPLED BY:

	Water Analysis														
RPT Date: Dec 02, 2021			C	UPLICATE	Ξ		REFEREN	ICE MA	TERIAL	METHOD	METHOD BLANK SPIKE			RIX SPI	KE
PARAMETER	Batch	Sample	Dup #1	Dup #2	RPD	Method Blank	Measured		ptable nits	Recovery	Lin	ptable nits	Recovery	Lie	ptable nits
		ld					Value	Lower	Upper		Lower	Upper		Lower	Upper
Peel Storm Sewer Use By-law - Ino	organics														
рН	3245263		7.61	7.73	1.6%	NA	103%	90%	110%						
Total Kjeldahl Nitrogen	3245716 3	3245716	0.77	0.69	11.0%	< 0.10	100%	70%	130%	101%	80%	120%	102%	70%	130%
Phenols	3235378		<0.001	<0.001	NA	< 0.001	109%	90%	110%	105%	90%	110%	115%	80%	120%
Total Phosphorus	3245716 3	8245716	9.91	10.6	6.7%	< 0.02	97%	70%	130%	99%	80%	120%	106%	70%	130%
Total Suspended Solids	3260570		<10	<10	NA	< 10	100%	80%	120%						
Total Cyanide	3244694		0.002	0.002	NA	< 0.002	116%	70%	130%	93%	80%	120%	98%	70%	130%
Total Arsenic	3248802		<0.015	<0.015	NA	< 0.015	88%	70%	130%	92%	80%	120%	98%	70%	130%
Total Cadmium	3248802		<0.001	<0.001	NA	< 0.001	100%	70%	130%	100%	80%	120%	105%	70%	130%
Total Chromium	3248802		<0.015	<0.015	NA	< 0.015	102%	70%	130%	102%	80%	120%	107%	70%	130%
Total Copper	3248802		<0.010	<0.010	NA	< 0.010	105%	70%	130%	110%	80%	120%	113%	70%	130%
Total Lead	3248802		<0.020	<0.020	NA	< 0.020	98%	70%	130%	106%	80%	120%	103%	70%	130%
Total Manganese	3248802		0.061	0.057	NA	< 0.020	95%	70%	130%	100%	80%	120%	98%	70%	130%
Total Mercury	3248939		<0.0002	<0.0002	NA	< 0.0002	104%	70%	130%	104%	80%	120%	97%	70%	130%
Total Nickel	3248802		<0.015	<0.015	NA	< 0.015	108%	70%	130%	107%	80%	120%	109%	70%	130%
Total Selenium	3248802		<0.002	0.004	NA	< 0.002	95%	70%	130%	96%	80%	120%	102%	70%	130%
Total Silver	3248802		<0.010	<0.010	NA	< 0.010	101%	70%	130%	111%	80%	120%	107%	70%	130%
Total Zinc	3248802		0.025	0.024	NA	< 0.020	100%	70%	130%	101%	80%	120%	102%	70%	130%

Comments: NA signifies Not Applicable.

If the RPD value is NA, the results of the duplicates are under 5X the RDL and will not be calculated.

Matrix spike: Spike level < native concentration. Matrix spike acceptance limits do not apply.

CBOD5								
Biochemical Oxygen Demand, Carbonaceous	3254918	181	172	5.1%	< 2	91%	70%	130%

Certified By:

Inis Verastegui

AGAT QUALITY ASSURANCE REPORT (V1)

Page 11 of 14

AGAT Laboratories is accredited to ISO/IEC 17025 by the Canadian Association for Laboratory Accreditation Inc. (CALA) and/or Standards Council of Canada (SCC) for specific tests listed on the scope of accreditation. AGAT Laboratories (Mississauga) is also accredited by the Canadian Association for Laboratory Accreditation Inc. (CALA) for specific tests tests. Accreditations are location and parameter specific. A complete listing of parameters for each location is available from www.cala.ca and/or www.scc.ca. The tests in this report may not necessarily be included in the scope of accreditation. RPDs calculated using raw data. The RPD may not be reflective of duplicate values shown, due to rounding of final results.



Method Summary

CLIENT NAME: THURBER ENGINEERING LTD

PROJECT: 30427

AGAT WORK ORDER: 21T834299

ATTENTION TO: Cary Zanatta

FINUSECT. 30427		ATTENTION TO.	Cary Zanalla								
SAMPLING SITE:		SAMPLED BY:									
PARAMETER	AGAT S.O.P	LITERATURE REFERENCE	ANALYTICAL TECHNIQUE								
Microbiology Analysis			1								
Escherichia coli	MIC-93-7010	EPA 1604	Membrane Filtration								
Fecal Coliform	MIC-93-7000	SM 9222 D	MF/INCUBATOR								
Trace Organics Analysis											
Methylene Chloride	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
cis-1,2-Dichloroethylene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
Chloroform	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
Benzene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
Trichloroethylene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
Toluene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
Tetrachloroethene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
trans-1,3-Dichloropropene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
Ethylbenzene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
1,1,2,2-Tetrachloroethane	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
1,2-Dichlorobenzene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
1,4-Dichlorobenzene	VOL-91-5001	modified from EPA 5030B & EPA 8260D modified from EPA 5030B & EPA	(P&T)GC/MS								
m & p-Xylene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
o-Xylene	VOL-91-5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
Xylenes (Total)	VOL-91-5001	modified from EPA 5030B & EPA 8260D	CALCULATION								
Toluene-d8	VOL-91- 5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
4-Bromofluorobenzene	VOL-91- 5001	modified from EPA 5030B & EPA 8260D	(P&T)GC/MS								
PCBs	ORG-91-5112	modified from EPA SW-846 3510C & 8082A	GC/ECD								
Decachlorobiphenyl	ORG-91-5112	modified from EPA SW846 3510C & 8082A	GC/ECD								
Di-n-butyl phthalate	ORG-91-5114	modified from EPA SW-846 3510C & 8270E	GC/MS								
Bis(2-Ethylhexyl)phthalate	ORG-91-5114	modified from EPA SW-846 3510C & 8270E	GC/MS								
2,4,6-Tribromophenol	ORG-91-5114	modified from EPA 3510C and EPA 8270E	GC/MS								
2-Fluorophenol	ORG-91-5114	modified from EPA 3510C and EPA 8270E	GC/MS								
Chrysene-d12	ORG-91-5114	modified from EPA 3510C and EPA 8270E	GC/MS								
phenol-d6 surrogate	ORG-91-5114	modified from EPA 3510C and EPA 8270E	GC/MS								



Method Summary

CLIENT NAME: THURBER ENGINEERING LTD

PROJECT: 30427

AGAT WORK ORDER: 21T834299

ATTENTION TO: Cary Zanatta

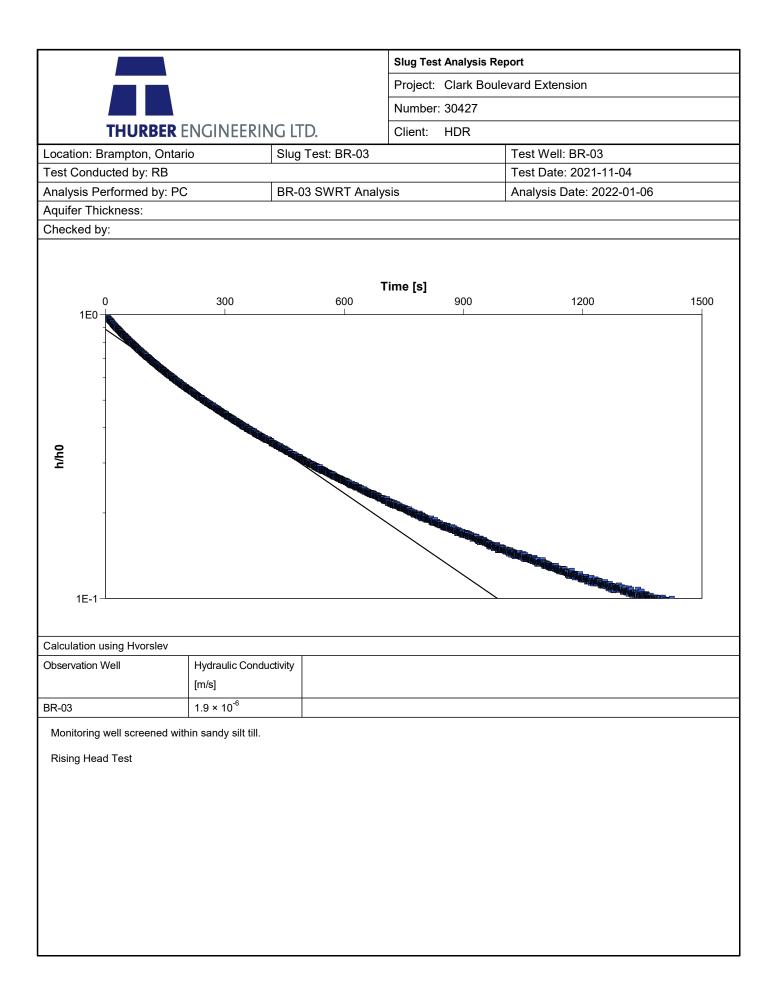
SAMPLING SITE:		SAMPLED BY:							
PARAMETER	AGAT S.O.P	LITERATURE REFERENCE	ANALYTICAL TECHNIQUE						
Water Analysis Biochemical Oxygen Demand, Carbonaceous	INOR-121-6023	SM 5210 B	INCUBATOR						
pH	INOR-93-6000	modified from SM 4500-H+ B	PC TITRATE						
Total Kjeldahl Nitrogen	INOR-93-6048	modified from EPA 351.2 and SM 4500-NORG D	LACHAT FIA						
Phenols	INOR-93-6072	modified from SM 5530 D	LACHAT FIA						
Total Phosphorus	INOR-93-6022	modified from SM 4500-P B and SM 4500-P E	SPECTROPHOTOMETER						
Total Suspended Solids	INOR-93-6028	modified from EPA 1684,ON MOECC E3139,SM 2540C,D	BALANCE						
Total Cyanide	INOR-93-6051	modified from MOECC E3015; SM 4500-CN- A, B, & C	TECHNICON AUTO ANALYZEF						
Total Arsenic	MET-93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						
Total Cadmium	MET -93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						
Total Chromium	MET-93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						
Total Copper	MET-93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						
Total Lead	MET-93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						
Total Manganese	MET-93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						
Total Mercury	MET-93-6100	modified from EPA 245.2 and SM 3112 B	² CVAAS						
Total Nickel	MET-93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						
Total Selenium	MET-93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						
Total Silver	MET-93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						
Total Zinc	MET-93-6103	modified from EPA 200.8, 3005A, 3010A & 6020B	ICP-MS						

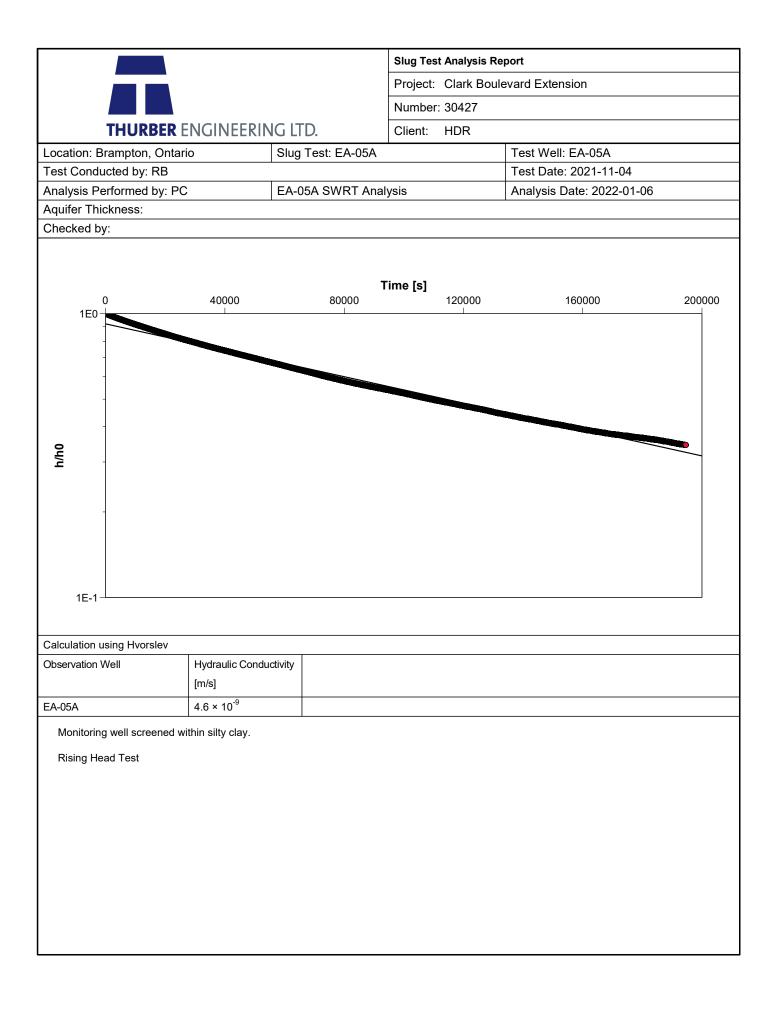
Chain of Custody Record		_			Ph: 90	05 712	sissaug .5100 web	sa, Or Fax: bearth	oopers A Itario L4 905 712 I.agatlat mans)	Z 1 2.51	/2 22	Wa	ork Order oler Quar	#: <u>2</u> ntity:		nly 8342 11.61	299	ξ1 (<u>/</u> .	4
Report Information: The bar Environment of the second		(Please of Rep Tab Di Di Di Soil Te Di Soil Te Di Rec	Regulatory Requirements: (Please check all applicable boxes) Regulation 153/04 Excess Soils R406 Tableindicate One Tableindicate One Indi/Com Tableindicate One Indi/Com ResyPark Agriculture Regulation 558 Soil Texture (check One) CCME Fine Is this submission for a			11						Custody Seal Intact: Notes: Turnaround Time (TAT) Required: Regular TAT 3 Business Days 0 R Date Required (Rush Surcharges May Apply): Please provide prior notification for rush TAT *TAT is exclusive of weekends and statutory holidays For 'Same Day' analysis, please contact your AGAT CPM							
Sampled By: AGAT Quote #: Please note: If quotation number is Invoice Information: Company: Contact: Address: Email:		e billed full price for a	1	Нв	nple Matrix Legend Biota Ground Water Oil Paint Soil Sediment Surface Water	Field Filtered - Metals, Hg, CrVI, DOC	& Inorganics o	- CrVI, CHB, CHWSB	BTEX, F1-F4 PHCs Analyze F4G if required \Box Yes \Box No			Landfill Disposal Characterization TCLP: 0.0	□vocs □ABNs □B(a)P □ PCBs s SPLP Rainwater Leach tals □ vocs □ svocs	laracteri als, BTE	Salt - EC/SAR	egin of feel Stan San			Potentially Hazardous or High Concentration (Y/N)
Sample Identification EA-05 EA-05 F	Date Sampled NJJ 33/2 NJJ 23/2	Time Sampled		Sample Matrix	Comments/ Special Instructions	¥/N	Metals	Metals -	BTEX, F Analyze	PAHS	Long Contraction	Fandfill	TICLP: CIMRAL Excess Solits SPLP: CIMRA	Excess	Salt - E	- Contraction of the second se			Potenti
Samples Relinquisited By (Print Name and Sign): Samples Relinquished By (Print Name and Sign): Samples Relinquished By (Print Name and Sign):		Date Date 1 c/2 4/ Date	Time		Samples Received By (Print Name and Sign): Samples Received By (Print Name and Sign): Samples Received By (Print Name and Sign):	en fe	7		Pink Co	opy -	Date Date Client	- 4/a	Time Time w Copy - /		White	Pag №: Т 1 Сору- AGAT	.26	of 261 ne issued: Main 14 of 14	

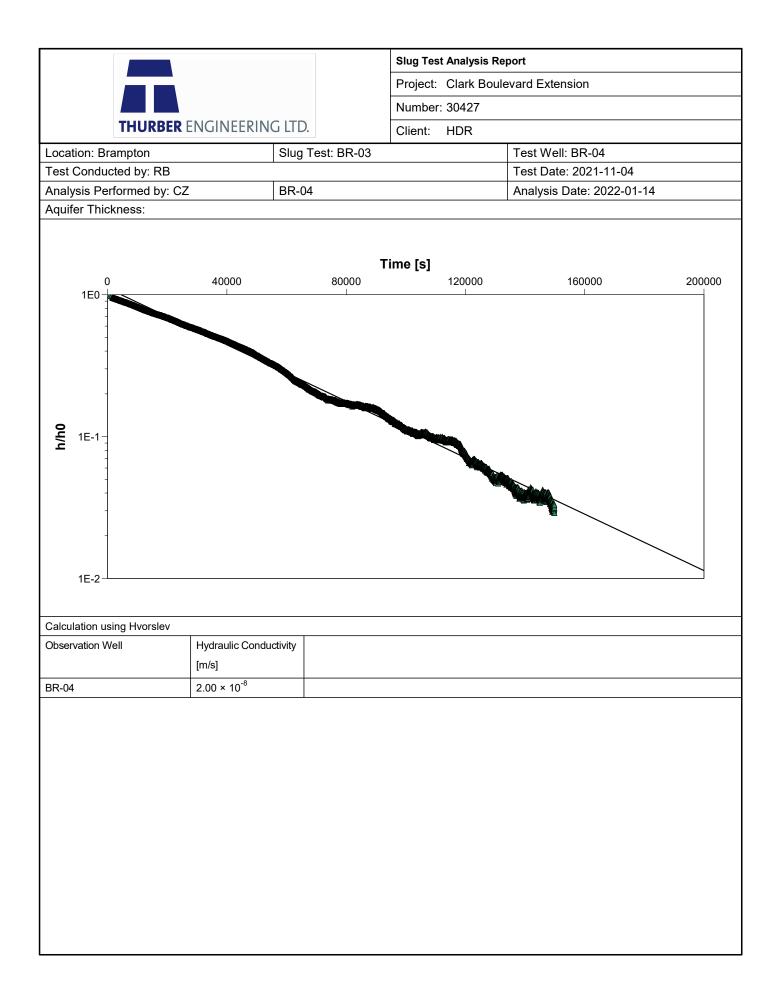


Appendix E

Single Well Response Test Analyses









Appendix F

Preliminary Dewatering Estimates

Parameter	Units	Box culvert crossing structure and channel realignment					
Geologic Unit to Dewater		Silty clay fill, silt and silt till, and possible sand layers					
Input Hydraulic Conductivity in m/s (K)	m/s	1.9E-06					
Hydraulic Conductivity converted to m/day	m/day	0.2					
Input height of groundwater pressure (H)	m	4.73					
Input dewatering height (h)	m	3.0					
Input length of excavation (x, a)	m	60					
Input width of excavation (b)	m	15					
Input/calculate radius of trench (rw or rs)	m	7.5					
Length to width ratio	unitless	4.0					
Net water table lowering	m	1.73					
Equation Type		Trench					
Radii of Influence							
Sichardt Equation (Ro based on K, H, h)	m	7					
Ro = Sichardt + (rw or rs)	m	15					
Calculated Flow Rate							
Base groundwater flow	L/day	19,000					
Partial Penetration Factor	unitless	1.00					
Safety factor on groundwater flow	unitless	3					
Groundwater flow with safety factor	L/day	57,000					
Rainfall entering excavation	mm	-					
Duration to remove rainfall	hours	-					
Flow rate to remove rainfall	L/day	-					
Budgeted peak flow rate	L/day	57,000					
=	L/s	0.7					
=	gal/min	9					

Dewatering Calculations for Unconfined Scenarios

Flow rate estimates rounded to nearest 1,000 L/day.